

Design Report 04: Twin Sea Lion

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Contents

List of Figures	ii
List of Tables	vi
I Introduction	1
II Addendum to Report 3	1
III Landing Gear Layout Design	1
III.A Sizing of the Landing Gear	1
III.B Location of the Landing Gear	2
III.B.1 Longitudinal Ground Clearance	2
III.B.2 Lateral Ground Clearance	2
III.B.3 Longitudinal Tip-Over	2
III.B.4 Lateral Tip-Over	4
III.C Gear Retraction Volume	5
IV Aircraft Dimensions and Three-View	6
IV.A Geometric Summary	6
IV.B Aircraft Three-View	8
V Moments of Inertia and Spin Characteristics	10
V.A Moments of Inertia	10
V.B Spin Characteristics	11
VI Stability and Control Derivative	13
VI.A Longitudinal Stability Derivatives	13
VI.B Lateral-Directional Stability Derivatives	13
VI.C Longitudinal Control Derivatives	14
VI.D Lateral-Directional Control Derivatives	14

VII Static Stability and One Engine Inoperative Analyses	15
VII.A Static Longitudinal Stability	15
VII.B Static Lateral-Directional Stability	15
VII.C One Engine Inoperative Stability Analysis	15
VIII Transfer Function and Flying Quality Analyses	15
VIII.A Transfer Function Analysis	15
VIII.A.1 Longitudinal Transfer Functions	15
VIII.A.2 Lateral-Directional Transfer Functions	17
VIII.A.3 Aileron Transfer Functions	18
VIII.A.4 Rudder Transfer Functions	18
VIII.B Flying Qualities Analysis	18
VIII.B.1 Longitudinal Flying Qualities	18
VIII.B.2 Lateral-Directional Flying Qualities	19
IX Design Changes Needed to Meet Mission Requirements or Improve Mission Performance	19
IX.A Conclusions	19
IX.B Recommended Design Changes	19
X Appendix	20
X.A AAA: Stability and Control Derivatives	20
X.B AAA: Static Stability and One Engine Inoperative Analyses	45
X.C AAA: Transfer Function and Flying Quality Analyses	46

List of Figures

1 Landing gear of similar airplanes	4
2 AAA results for tip-over conditions	5
3 Top view of the Twin Sea Lion	8
4 Side view of the Twin Sea Lion	9

5	Front view of the Twin Sea Lion	9
6	AAA inertia inputs	11
7	Spin recoverability prediction, with the Twin Sea Lion's location marked	12
8	Airspeed response to elevator deflection transfer function	16
9	Angle of attack response to elevator deflect transfer function	16
10	Flight path angle response to elevator deflection transfer function	17
11	Short period response is slightly outside level 1 requirements	18
12	Wing lift curve slope	20
13	Wing lift coefficient at zero angle of attack	21
14	Horizontal stabilizer lift curve slope	21
15	Horizontal stabilizer downwash gradient	21
16	Horizontal stabilizer downwash angle	22
17	Horizontal stabilizer lift coefficient at zero angle of attack	22
18	Vertical stabilizer sidewash gradient	22
19	Vertical stabilizer downwash gradient	23
20	Vertical stabilizer downwash angle	23
21	Wing lift coefficient	23
22	Wing drag coefficients	24
23	Wing aerodynamic center	24
24	Horizontal stabilizer aerodynamic center	24
25	Vertical stabilizer aerodynamic center	24
26	Aerodynamic center shift due to fuselage effects	25
27	Power-off dynamic pressure ratio	25
28	Elevator related derivatives	25
29	Horizontal tail lift coefficient	25
30	Steady state lift coefficients	26
31	Angle of attack related derivatives	26

32	Aircraft aerodynamic center	26
33	Steady state lift coefficient	27
34	Steady state flight coefficients	27
35	Steady state drag polar calculations	27
36	Steady state thrust	27
37	Steady state pitching moment	28
38	Steady state pitching moment	28
39	Speed related derivatives	28
40	Speed related derivatives	28
41	Speed related derivatives	29
42	Speed related derivatives	30
43	Speed related derivatives	30
44	Angle of attack related derivatives	31
45	Angle of attack related derivatives	31
46	Angle of attack related derivatives	31
47	Angle of attack related derivatives	32
48	Angle of attack rate related derivatives	32
49	Angle of attack rate related derivatives	33
50	Angle of attack rate related derivatives	33
51	Pitch rate related derivatives	33
52	Pitch rate related derivatives	34
53	Pitch rate related derivatives	34
54	Fuselage geometry	35
55	Sideslip related derivatives	35
56	Sideslip related derivatives	35
57	Sideslip related derivatives	36
58	Sideslip related derivatives	36

59	Sideslip related derivatives	37
60	Horizontal stabilizer drag coefficient	37
61	Sideslip rate related derivatives	37
62	Sideslip rate related derivatives	38
63	Sideslip rate related derivatives	38
64	Sideslip related derivatives	39
65	Sideslip related derivatives	39
66	Roll rate related derivatives	40
67	Roll rate related derivatives	40
68	Roll rate related derivatives	41
69	Yaw rate related derivatives	41
70	Yaw rate related derivatives	41
71	Yaw rate related derivatives	42
72	Angle of attack related derivatives	42
73	Elevator related derivatives	42
74	Elevator related derivatives	42
75	Elevator related derivatives	43
76	Aileron related derivatives	43
77	Aileron related derivatives	43
78	Aileron related derivatives	44
79	Rudder related derivatives	44
80	Rudder related derivatives	44
81	Rudder related derivatives	44
82	Angle of attack related derivatives	45
83	Sideslip related derivatives	45
84	Rudder related derivatives	45
85	One engine out at cruise altitude and speed	46

86	One engine out at takeoff altitude and speed	46
87	Longitudinal transfer functions, frequencies, and damping	46
88	Lateral-directional transfer functions, frequencies, and damping response to ailerons	47
89	Lateral-directional transfer functions, frequencies, and damping response to rudder	47
90	Longitudinal mode frequencies, phugoid and short period flying quality levels	47
91	Roll mode performance and flying quality level	48
92	Spiral and dutch roll fling quality levels	48
93	Spiral and dutch roll fling quality levels	48

List of Tables

1	Summary of main gear and tire dimensions	1
2	Summary of nose gear and tire dimensions	1
3	Summary and clearance and tip-over requirements	1
4	Expanded gear dimensions.	6
5	Geometric design variables	7
6	All longitudinal stability derivatives	13
7	All lateral stability derivatives	14
8	All longitudinal control derivatives	14
9	All lateral control derivatives	14

Nomenclature

AAA	=	Advanced Aircraft Analysis Program
AR_W	=	Wind aspect ratio
b_w	=	Wing span
c_w	=	Wing chord
D_{t_n}	=	Nosewheel tire diameter
D_{t_M}	=	Main gear tire diameter
d_{ns}	=	Nose strut diameter
d_{ms}	=	Main strut diameter
$d_{retract}$	=	Gear bogey diameter while retracted
i_w	=	Wing incidence angle
l_f	=	Fuselage length
l_m	=	Length from x_{cg} to main gear
l_n	=	Length from x_{cg} to nose gear
n_m	=	Number of main gear
P_n	=	Maximum static load per nose bogey
P_m	=	Maximum static load per main bogey
S_W	=	Wing area
S_h	=	Horizontal stabilizer area
S_v	=	Vertical stabilizer area
$TDPF$	=	Tail Damping Power Factor
W_{TO}	=	Takeoff weight
$w_{retract}$	=	Gear bogey width while retracted
X	=	Distance of a component from the nose of the aircraft
Y	=	Distance of a component from the centerline of the aircraft
Z	=	Distance of a component from the belly of the aircraft
λ_w	=	Wing sweep angle

$\Lambda_{c/4w}$ = Quarter chord sweep angle

Γ_W = Wing dihedral angle

ϵ_W = Wing twist angle

I. Introduction

This is the final report on development progress of the Twin Sea Lion. This report covers landing gear configuration, ground clearance and tipover calculations, spin characteristics and the flying qualities of the Twin Sea Lion.

II. Addendum to Report 3

Fuel x_{cg} was incorrectly placed at 22 ft while the wing x_{cg} was at 23 ft. Since the fuel cannot be before the wing, the fuel had to be moved back. This correction also improved the stability from 44% to 41%.

III. Landing Gear Layout Design

Tables 1, 2, and 3 summarize the results of the gear layout section.

Table 1 Summary of main gear and tire dimensions

D_{t_m} [in]	b_{t_m} [in]	n_{mt}	l_m [ft]	P_m [lb]	P_m [%]	d_{ms} [ft]	L_{S_m} [ft]
30	9	2	3	16,152	42.86	0.3587	6.15

Table 2 Summary of nose gear and tire dimensions

D_{t_n} [in]	b_{t_n} [in]	n_{nt}	l_n [ft]	P_n [lb]	P_n [%]	d_{ns} [ft]	L_{S_n} [ft]
23.4	6.5	2	18	5384.1	14.29	0.2244	5.36

Table 3 Summary and clearance and tip-over requirements

Requirement	Sea Lion Value [deg]	Relation	Requirement [deg]	Satisfaction
Longitudinal Ground Clearance	14.9	\neq	15	F
Lateral Ground Clearance	15.68	>	5	T
Longitudinal Tip-Over	12.86	\neq	15	F
Lateral Tip-Over	51.8	<	55	T

A. Sizing of the Landing Gear

Designers chose a tricycle configuration as it allows the most passenger comfort while the plane is on the ground. A tricycle configuration also makes the plane easier to steer on the ground. These gears will be retractable, with three total struts. The nose gear and main gear each have two tires per strut. Tires were selected to be similar to other regional turboprops of a similar weight. These tires will have a dual arrangement. Definitions of P_n (Equation 1) and P_m (Equation 2) come from Presentation 26[8]. For the Twin Sea Lion, $l_n = 18$ ft $l_m = 3$ ft, so $P_n = 5384.1$ lb = 14.29%

and $P_m = 16152 \text{ lb} = 42.86\%$.

$$P_n = \frac{W_{TO}l_m}{l_m + l_n} \quad (1)$$

$$P_m = \frac{W_{TO}l_n}{n_m(l_m + l_n)} \quad (2)$$

B. Location of the Landing Gear

Locations were originally chosen in order to put 10% of the weight on the nose gear with the main gear slightly behind the aircraft cg. Changes made in order to meet longitudinal ground clearance requirements took the nose gear loading up to 14.28%. This placed the main gear 3 ft behind the aircraft cg and the nose gear 18 ft in front of the aircraft cg.

1. Longitudinal Ground Clearance

The nose struts are 17 feet ahead of the apex of the wing and the empennage begins to sweep upwards 21 feet behind the main gear. The height above the ground of this corner is determined by the length of the struts so these struts were designed to ensure the required 15 degrees of clearance[8]. Clearance from the belly is calculated in Equation 3 as 5.36 feet. The belly is 9.5 inches below where the struts will begin, so the main landing gear struts are 6.15 feet long.

$$h = 21 \tan(\alpha) = 21 \tan(15 \text{ deg}) = 5.36 \text{ ft} \quad (3)$$

2. Lateral Ground Clearance

With 5.36 feet of clearance below the belly at the main landing gear, 32 feet from the main landing gear to the wingtip, and a wingtip height of 8.94 feet, the wingtips have a clearance of 15.68 degrees from the ground location of the main gear. This is greater than the 5 degrees required[8]. Propeller strikes are not a risk because the propellers are directly above the main gear.

3. Longitudinal Tip-Over

Longitudinal tip-over depends on the gear placement and tire separation as input to AAA in Figure 2. Nose strut diameter is 0.2244 feet and main strut diameter is 0.3587 feet as determined from Equations 4 and 5 respectively. As determined from the longitudinal clearance requirement, the main gear struts are 5.36 feet + 9.5 in = 6.15 ft long. The

nose gear strut is 5.36 feet long.

$$d_{ns} = (0.041 + 0.0025\sqrt{P_n}) = 0.2244 \quad (4)$$

$$d_{ms} = (0.041 + 0.0025\sqrt{P_m}) = 0.3587 \quad (5)$$

With two wheels on each strut align in the y direction, lateral tip-over depends on the y separation of the wheels. This separation needs to be slightly more than the sum of two half thicknesses of the tires and the strut diameter as seen in Equation 6.

$$Styn = 1.05(t_n + d_{ns}) = 0.8044 \quad (6)$$

$$Stym = 1.05(t_m + d_{ms}) = 1.1642 \quad (7)$$

Table 9.1 Typical Landing Gear Wheel Data ($n_s = 2$)

Type	W_{TO} lbs	Main Gear				Nose Gear			
		$D_t \times b_t$	$2P_m/W_{TO}$	PSI	n_{mt}	$D_t \times b_t$	P_n/W_{TO}	PSI	n_{nt}
Homebuilt	600	13x5	0.80	25	1	9x3.4	0.17	25	1
	1,200	12x5	0.78	45	1	12x5	0.22	45	1
	3,300	16x6	0.87	45	1	16x6	0.13	45	1
Single Engine Prop. Driven	1,600	15x6	0.80	18	1	15x5	0.20	28	1
	2,400	17x6	0.84	19	1	12.5x5	0.16	22	1
	3,800	16.5x6	0.84	55	1	14x5	0.16	49	1
Twin Engine Prop. Driven	5,000	16x6	0.83	55	1	16x6	0.17	40	1
	8,000	22x6.5	0.88	75	1	17x6	0.12	40	1
	12,000	26.6x7	0.84	82	1	19.3x6.6	0.16	82	1
Agricultural	3,000	22x8	0.95	35	1	9x3.5*	0.05*	55*	1*
	7,000	24x8.5	0.92	35	1	12.4x4.5*	0.08*	50*	1*
	10,000	29x7.5	0.85	35	1	25x7	0.15	35	1
*Note: these are tailwheel data									
Regional Turbo- propeller Driven Airplanes	12,500	18x5.5	0.89	105	2	22x6.75	0.11	57	1
	21,000	24x7.25	0.90	85	2	18x5.5	0.10	65	2
	26,000	36x11	0.92	40	1	20x7.5	0.08	40	1
	44,000	30x9	0.93	107	2	23.4x6.5	0.07	77	2
Business Jets	12,000	22x6.3	0.93	90	1	18x5.7	0.07	120	1
	23,000	27.6x9.3	0.95	155	1	17x5.5	0.05	50	2
	39,000	26x6.6	0.92	208	2	14.5x5.5	0.08	130	2
	68,000	34x9.25	0.93	174	2	21x7.25	0.07	113	2

Fig. 1 Landing gear of similar airplanes

With all this input into AAA, Figure 2 gives $\phi_{gear_{cg}} = 12.86$ deg. The requirement for longitudinal tip-over is that $\phi_{gear_{cg}} > 15$ [8]. This requirement is not met but is close enough to accept for the first round of design.

$$\phi = 12.86 \text{ deg} \not> 15 \text{ deg} \quad (8)$$

4. Lateral Tip-Over

Lateral tip-over is determined by the same AAA module as longitudinal tip-over. Figure 2 gives $\psi = 51.8$ deg. In order to pass this requirement $\psi \leq 55$ deg[8]. This requirement is easily satisfied. The Sea Lion will not tip-over laterally.

$$\psi = 51.8 \text{ deg} < 55 \text{ deg} \quad (9)$$

Landing Gear Geometry: Flight Condition 1

Input Parameters					
X _{cg}	24.32	ft	Y _{cg}	-0.11	ft
Z _{cg}	2.95	ft			
Output Parameters					
X _{gear_forw}	6.00	ft	Z _{gear_forw}	-6.33	ft
Y _{gear_forw}	0.00	ft	X _{gear_aft}	26.50	ft
Z _{gear_aft}	9.10	ft			
Ψ	51.8	deg	Z _{gear_crit}	-6.60	ft
Φ _{gear_cg_e}	9.58	deg			
X _{gear_crit}	26.50	ft	Φ _{gear_cg}	12.86	deg
				Coordinates Defined	
Landing Gear Table					
#	Landing Gear	N _{side-by-side}	N _{inline}	D _{wheel} ft	w _{wheel} ft
1	Nose Gear: Down	2	1	1.95	0.54
2	Main Gear: Down	2	1	2.50	0.75
3	Main Gear: Down	2	1	2.50	0.75
	X _{wheel} ft	Y _{wheel} ft	Z _{wheel} ft	S _B _{wheel} ft	S _T _{wheel} ft
	6.00	0.00	-5.35	0.00	0.80
	26.50	9.10	-5.35	0.00	1.16
	26.50	-9.10	-5.35	0.00	1.16

Fig. 2 AAA results for tip-over conditions

C. Gear Retraction Volume

Expansions of the tires in inches are given by Equations 10 and 11 for tire width and diameter respectively[8]. Total retraction volume is estimated using these new dimensions and modeling the set of tires as a cylinder.

$$w_{retract} = w + 0.04w + 3 \quad (10)$$

$$d_{retract} = d + 0.1d + 3 \quad (11)$$

Based on the above, each main gear tire was assumed to expand to a diameter of 36 inches and width of 12.36 inches

Table 4 Expanded gear dimensions.

Gear	Individual D [in]	Individual W [in]	Total D [ft]	Total W [ft]	Volume [ft^3]
Nose	26.634	9.76	2.2195	1.851	7.1616
Main	36	12.36	3	2.4187	17.0967

in cruise. By approximating the two tires and the diameter of the gear strut as a cylinder with length equal to twice the width of the wheel plus the strut diameter and a diameter equal to the tire's expanded diameter, the retracted volume of the main gear is calculated to be the following on each side and is tabulated in Table 4.

$$V_{h_main} = 17.0967 \text{ } ft^3 \quad (12)$$

From Report 02[2], the Twin Sea Lion requires 10,679 pounds of fuel and the wings have room for 20,559 pounds or $407.76 \text{ } ft^3$ of fuel. This leaves $195.96 \text{ } ft^3$ across both wings or $97.98 \text{ } ft^3$ in each wing for things other than fuel. The retracted gear would take up 17.4% of the remaining gear volume, leaving a very reasonable 82.6% of the non-fuel wing volume for other materials like tanks, wires, and hydraulics.

The nose gear expands in a similar manner. Each expanded tire was calculated as 26.634 inches in diameter and 9.76 inches in width. Again accounting for both tires and the diameter of the nose gear strut, the retracted volume of the nose gear is as follows.

$$V_{h_nose} = 7.1615 \text{ } ft^3 \quad (13)$$

The total diameter of the nose gear cylinder is 2.2195 ft and the total length is 1.851 ft. From Report 02[2], the back half of the cockpit has 17.55 in or 1.4625 ft from the floor to the outer shell. This is too small for the nose gear to fit either way so the gear will be retracted as far as possible and a clam shell used to cover the remaining.

IV. Aircraft Dimensions and Three-View

A. Geometric Summary

Wing design variables and fuselage length were determined in Report 02[2], and tail areas were determined in Report 03[3].

Table 5 Geometric design variables

$S_W [ft^2]$	$b_w [\text{ft}]$	AR_W	$c_w [\text{ft}]$	λ_W	$\Lambda_{c/4w} [\text{°}]$	$\Gamma_W [\text{°}]$	$i_W [\text{°}]$	$\epsilon_W [\text{°}]$	$l_f [ft]$	$S_h [ft^2]$	$S_v [ft^2]$
837	81.8	8	10.16	0.6	0	5	-1	0	47.58	190.0	137.0

B. Aircraft Three-View

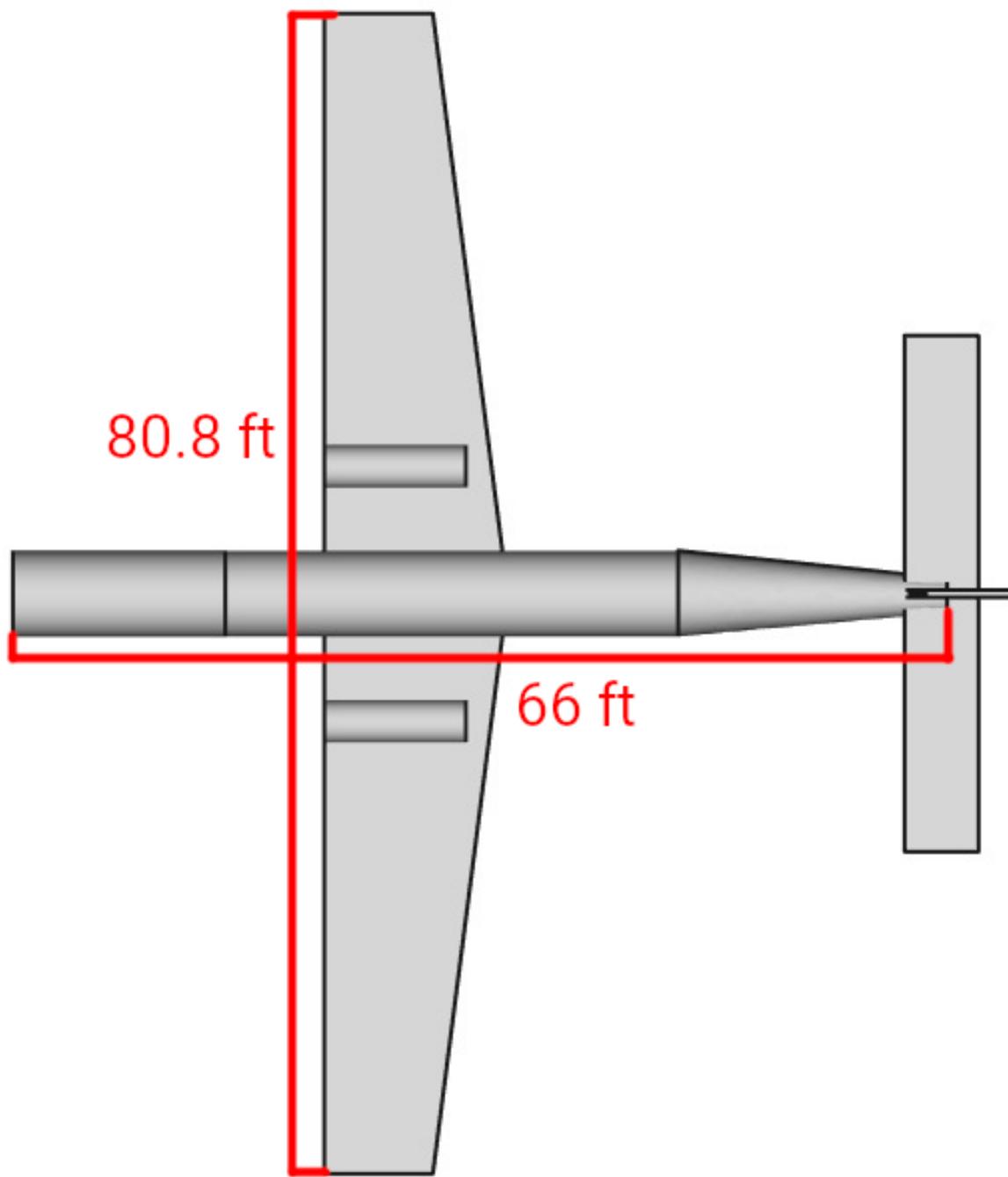


Fig. 3 Top view of the Twin Sea Lion

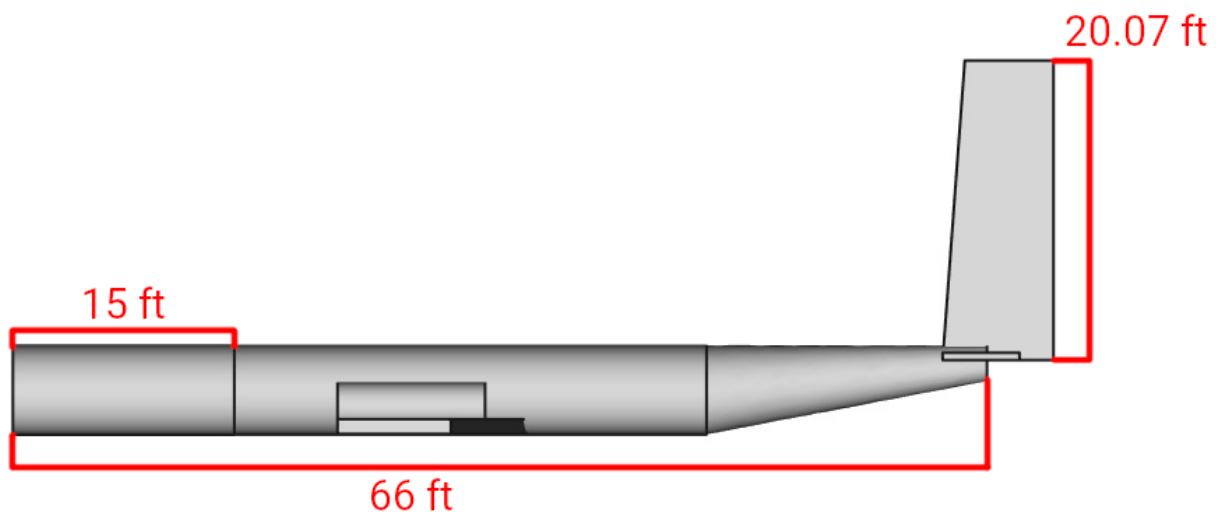


Fig. 4 Side view of the Twin Sea Lion

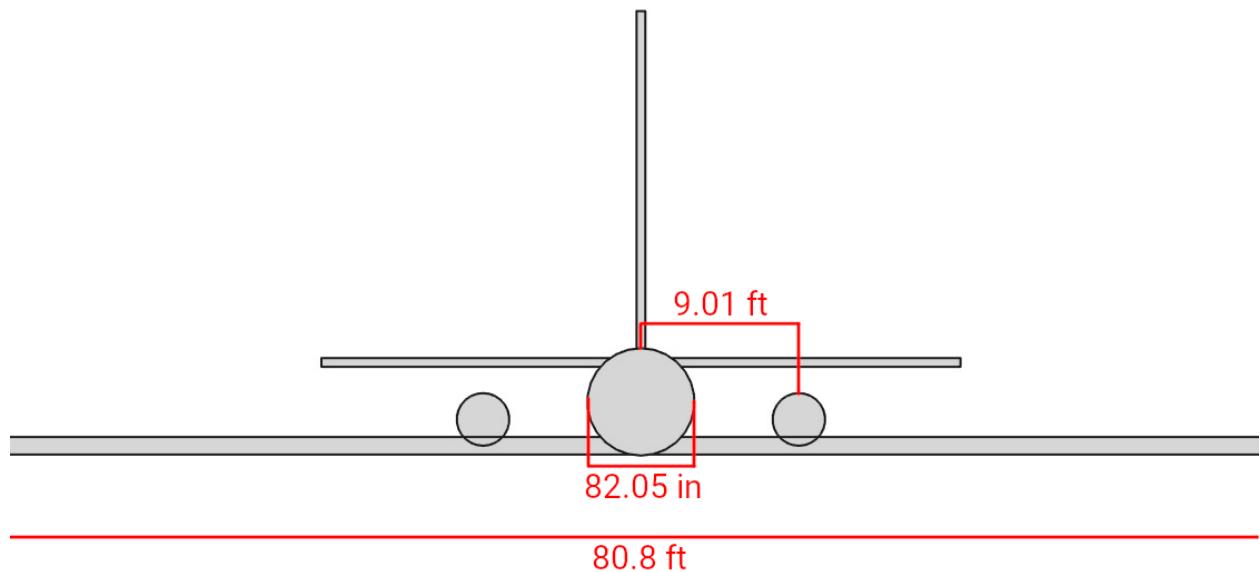


Fig. 5 Front view of the Twin Sea Lion

Note that while the length of the cockpit has been included in this model, the precise details are not included and it is simply replaced with a cylinder.

V. Moments of Inertia and Spin Characteristics

A. Moments of Inertia

The empty weight table seen in Figure 6 was populated with all empty weight groups and supplemented with the aircraft load split as much as possible with the available boxes. Note that the component names in the table were ignored in order to fit as many parts of the aircraft into the table as possible.

The actual names associated with each item are as follows.

- | | |
|---------------------------|--------------------------|
| 1) Furnishings | 12) Nose gear |
| 2) Other fixed equipment | 13) Main gear 1 |
| 3) Engine 1 | 14) Main gear 2 |
| 4) Engine 2 | 15) Fuel 1 |
| 5) Propeller 1 | 16) Fuel 2 |
| 6) Propeller 2 | 17) Cargo |
| 7) Wing 1 | 18) Baggage |
| 8) Wing 2 | 19) Crew |
| 9) Fuselage | 20) Trapped fuel and oil |
| 10) Horizontal Stabilizer | 21) Passenger group 1 |
| 11) Vertical Stabilizer | 22) Passenger group 2 |

Items split into groups 1 and 2 denote equipment that is on the right and left side of the aircraft respectively.

Class II Empty Weight Moment of Inertia: Flight Condition 1									
Input Parameters									
X_{cg_E}	24.80	ft	Y_{cg_E}	0.00	ft	Z_{cg_E}	3.47	ft	
Output Parameters									
I_{xx_B}	200121.1	slug-ft ²	I_{yy_B}	51880.2	slug-ft ²	I_{zz_B}	245693.0	slug-ft ²	
							I_{xz_B}	4375.6	slug-ft ²

Class II Empty Weight Moment of Inertia Table								
Component	Weight lb	I_{xx_B} slug-ft ²	I_{yy_B} slug-ft ²	I_{zz_B} slug-ft ²	I_{xz_B} slug-ft ²	X_{cg} ft	Y_{cg} ft	Z_{cg} ft
Wing	83.4					41.63	1.96	4.21
Horizontal Tail	5192.0					21.41	0.00	3.50
Vertical Tail	1896.3					23.80	9.00	3.80
Fuselage	1896.3					23.80	-9.00	3.80
Nose Landing Gear	901.8					20.00	9.00	3.80
Main Landing Gear	901.8					20.00	-9.00	3.80
Propeller	1693.1					23.00	18.75	3.50
Turboprop Engine	1693.1					23.00	-18.75	3.50
Fuel System	4455.6					21.41	0.00	3.50
Air Induction System	445.6					62.00	0.00	6.00
Propulsion System	267.3					62.00	0.00	16.00
Flight Control System	245.9					6.00	0.00	0.98
Hydraulic and Pneumatic System	696.9					27.00	9.10	2.38
Instruments/Avionics/Electronics	696.9					27.00	-9.10	2.38
Electrical System	5348.6					23.00	18.75	2.00
Air Cond./Press./Icing System	5348.6					23.00	-18.75	2.00
Oxygen System	2020.0					33.00	-2.00	0.00
Auxiliary Power Unit	605.0					28.92	0.00	3.00
Furnishings	525.0					12.05	-0.56	5.00
Cargo Handling Equipment	188.4					21.41	0.00	3.50
Operational Items	875.0					28.92	21.57	5.00
Other Items	875.0					28.92	-21.57	5.00

Fig. 6 AAA inertia inputs

B. Spin Characteristics

The spin recovery criterion is described in Equation 14. S_{R_1} is the usable area of the rudder above the horizontal stabilizer. L_1 is the length from aircraft cg to the center of S_{R_1} . S_{R_2} and L_2 are similarly related. These parameters are taken from Presentation 27[9]

$$SRC = \frac{I_x - I_y}{b^2(W/g)} \quad (14)$$

$$TDPF = (TDR)(URVC) \quad (15)$$

$$TDR = \frac{S_F L^2}{S_w (b/2)^2} \quad (16)$$

$$URVC = \frac{S_{R_1} L_1 + S_{R_2} L_2}{S_w (b/2)} \quad (17)$$

$$\mu = \frac{W/S}{\rho g b} \quad (18)$$

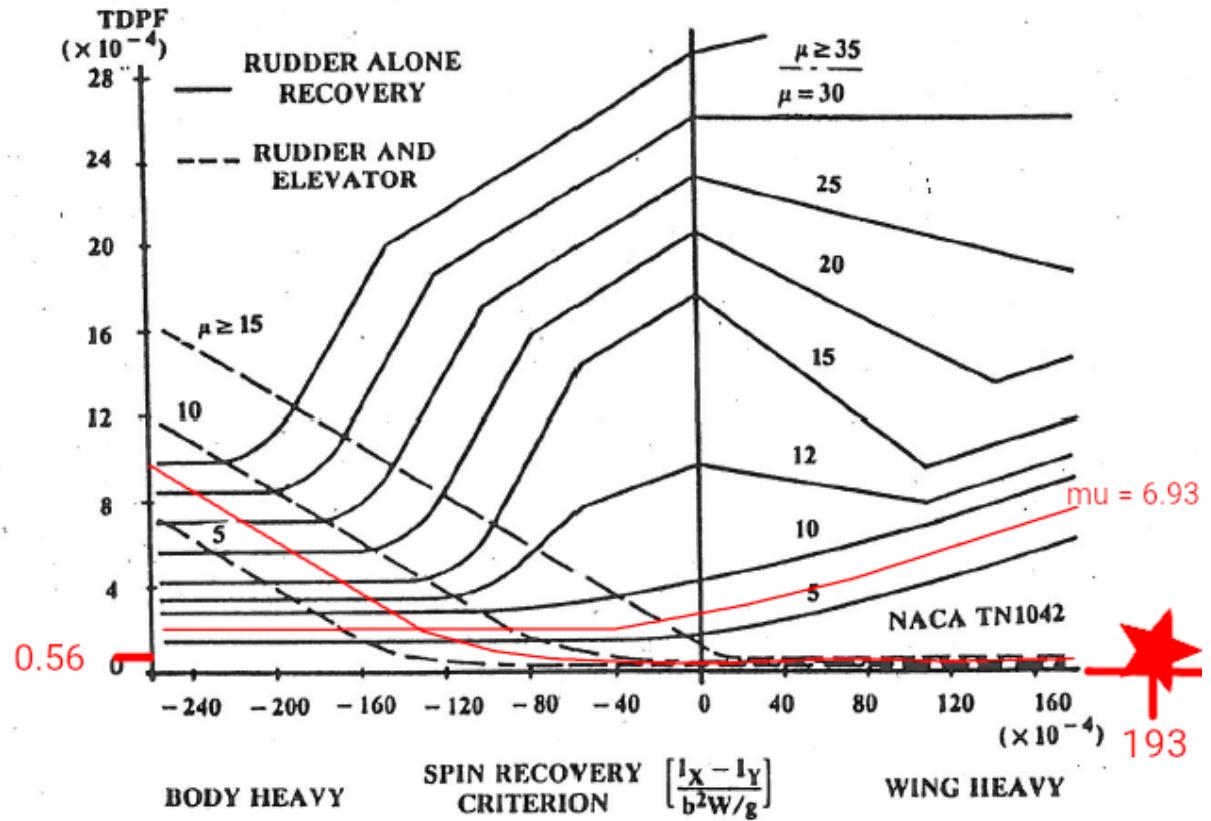


Fig. 16.31. Spin recovery criteria.

Fig. 7 Spin recoverability prediction, with the Twin Sea Lion's location marked

Thanks to the tall, single vertical stabilizer, $S_R = 8.19 \text{ ft}^2$ and $L_R = 42 \text{ ft}$ at most aft CG. A small amount of the vertical stabilizer aside from the rudder is not blanketed, so $S_F = 5 \text{ ft}^2$ and $L_f = 39 \text{ ft}$. From these, $TDPF = 0.566 \times 10^{-4}$, $\mu = 6.93$ at sea level, and $SRC = 193 \times 10^{-4}$. From the above graphic, it is apparent that the Twin Sea Lion is very

wing heavy and because its rudder is blanketed almost entirely by dirty air, it has next to no chance of recovery if a spin is encountered. However, this is acceptable for a FAR 25 certified aircraft.

In addition, the authors note that while no testing is planned, it may be possible to arrest a spin with differential thrust.

VI. Stability and Control Derivative

A. Longitudinal Stability Derivatives

All longitudinal stability derivatives and coefficients were determined from AAA using handout #2[5] and results from handout #1[4]. AAA printouts for this section can be found in Figures 33 through 54, with background calculations in Figures 12 through 32.

Table 6 All longitudinal stability derivatives

Steady State Coefficients	C_{L_1}	C_{D_1}	$C_{T_{x_1}}$	$C_{m_{T_1}}$	C_{m_1}
	0.1076	0.0177	0.0177	-0.0013	0.0013
Aerodynamic Speed Derivatives	C_{D_u}	C_{L_u}	C_{m_u}	$C_{T_{x_u}}$	$C_{m_{T_u}}$
	0	0.0586	0.0106	-0.0531	0.0038
Angle of Attack Derivatives	C_{D_α}	C_{L_α}	C_{m_α}	$C_{m_{T_\alpha}}$	
	0.0972	6.1586	-3.5082	-0.0251	
Change of Angle of Attack Derivatives	$C_{D'_\alpha}$	$C_{L'_\alpha}$	$C_{m'_\alpha}$		
	0	3.6077	-12.7779		
Pitch Rate Derivatives	C_{D_q}	C_{L_q}	C_{m_q}		
	0	14.1354	-32.5032		

B. Lateral-Directional Stability Derivatives

Calculations for lateral-directional stability derivatives were done in AAA as described in handout #2 with printouts from Figures 55 through 71.

Table 7 All lateral stability derivatives

Aerodynamic sideslip derivatives	C_{y_β}	C_{l_β}	C_{n_β}	$C_{Y_{T_\beta}}$	$C_{n_{T_\beta}}$
	-0.9179	-0.3025	0.3995	0	0
Sideslip rate derivatives	$C_{y'_\beta}$	$C_{l'_\beta}$	$C_{n'_\beta}$		
	-0.0066	-0.0017	-0.0029		
Roll rate derivatives	C_{y_p}	C_{l_p}	C_{n_p}		
	-0.1342	-0.5259	-0.0193		
Yaw rate derivatives	C_{y_r}	C_{l_r}	C_{n_r}		
	0.7794	0.2663	-0.3678		

C. Longitudinal Control Derivatives

Table 8 All longitudinal control derivatives

Longitudinal control derivatives were calculated in AAA, resulting in Figures 72 through 75.

Longitudinal control derivatives	$C_{D_{\delta_e}}$	$C_{L_{\delta_e}}$	$C_{M_{\delta_e}}$
	0.0087	0.5482	-1.9416

D. Lateral-Directional Control Derivatives

Lateral-directional control derivatives were calculated in AAA as shown in Figures 76 through 81.

Table 9 All lateral control derivatives

Aileron control derivatives	$C_{y_{\delta_a}}$	$C_{L_{\delta_a}}$	$C_{n_{\delta_a}}$
	0	0.1629	-0.0044
Rudder control derivatives	$C_{y_{\delta_r}}$	$C_{L_{\delta_r}}$	$C_{n_{\delta_r}}$
	0.2717	0.0726	-0.1380

VII. Static Stability and One Engine Inoperative Analyses

A. Static Longitudinal Stability

With the updates from Handouts #1 through #4, the Twin Sea Lion now has a static margin $SM = 56\%$. This is far in excess of the typical 10% to 15% that most aircraft have. The most forward cg in cruise comes directly after adding baggage when the airplane takes off. This gives 24.27 ft. The most aft cg in cruise comes after unloaded fuel and gives 24.83 ft. The initial calculations were done at 24.32 ft. The static margin at the most forward cg is then 57.44% and the is 52.07%. All of these are stable but none of them are acceptable for controllability. Static margin could be improved by a revised horizontal stabilizer or a complete overhaul of fuselage design.

B. Static Lateral-Directional Stability

From Table 7, $C_{n\beta} = 0.3995$. This is suitably positive for positive stability and so is an acceptable value for lateral directional stability.

C. One Engine Inoperative Stability Analysis

Thanks to substantial rudder area, the Twin Sea Lion appears to have no issues with an engine out. As seen in Figures 85 and 86, the Twin Sea Lion needs to only deflect its rudder by 0.28 degrees at cruise altitude and speed, or 0.82 degrees at takeoff speed and altitude. However, V_{mc} is 420 knots at cruise and 168 knots at takeoff. Both these numbers are above the normal flying speeds of the aircraft. This is something of a contradiction, because the rudder deflections given are not anywhere near their maximums. This indicates that in reality the rudder could be more useful than AAA is calculating.

VIII. Transfer Function and Flying Quality Analyses

A. Transfer Function Analysis

1. Longitudinal Transfer Functions

Longitudinal transfer functions were determined through AAA in Figure 87. The following printouts, Figures 8 through 10 through the actual transfer functions as produced by AAA.

Longitudinal Transfer Function

Polynomial Form:

$$\frac{u(s)}{e(s)} = \frac{-565\ 5055\ s^3 - 6591\ 7688\ s^2 + 867350\ 4462\ s + 924232\ 6193}{594\ 2409\ s^4 + 6860\ 1311\ s^3 + 58549\ 8487\ s^2 + 595\ 4493\ s + 164\ 2356}$$

Factored Form:

$$\frac{u(s)}{e(s)} = \frac{-565\ 5055\ (s - 34\ 3625)(s + 44\ 9610)(s + 1\ 0578)}{594\ 2409\ (s^2 + 11\ 5345\ s + 98\ 4123)(s^2 + 0\ 0099\ s + 0\ 0028)}$$

$$K_{\text{gain}} = 5627\ 480478$$

Fig. 8 Airspeed response to elevator deflection transfer function

Longitudinal Transfer Function

Polynomial Form:

$$\frac{\alpha(s)}{e(s)} = \frac{-60\ 3020\ s^3 - 29782\ 3990\ s^2 - 294\ 5643\ s - 83\ 8327}{594\ 2409\ s^4 + 6860\ 1311\ s^3 + 58549\ 8487\ s^2 + 595\ 4493\ s + 164\ 2356}$$

Factored Form:

$$\frac{\alpha(s)}{e(s)} = \frac{-60\ 3020\ (s + 493\ 8772)(s^2 + 0\ 0099\ s + 0\ 0028)}{594\ 2409\ (s^2 + 11\ 5345\ s + 98\ 4123)(s^2 + 0\ 0099\ s + 0\ 0028)}$$

$$K_{\text{gain}} = -0\ 510442$$

Fig. 9 Angle of attack response to elevator deflect transfer function

Longitudinal Transfer Function

Polynomial Form:

$$\frac{\theta(s)}{e(s)} = \frac{-300268919 s^2 - 292547017 s - 2943308}{5942409 s^4 + 68601311 s^3 + 585498487 s^2 + 5954493 s + 1642356}$$

Factored Form:

$$\frac{\theta(s)}{e(s)} = \frac{-300268919 (s + 0.9641)(s + 0.0102)}{5942409 (s^2 + 11.5345 s + 98.4123)(s^2 + 0.0099 s + 0.0028)}$$

$$K_{\text{gain}} = -1.792125$$

Fig. 10 Flight path angle response to elevator deflection transfer function

2. *Lateral-Directional Transfer Functions*

Lateral transfer functions were determined through AAA in Figure 88 for aileron and 89 for rudder.

3. Aileron Transfer Functions

4. Rudder Transfer Functions

B. Flying Qualities Analysis

1. Longitudinal Flying Qualities

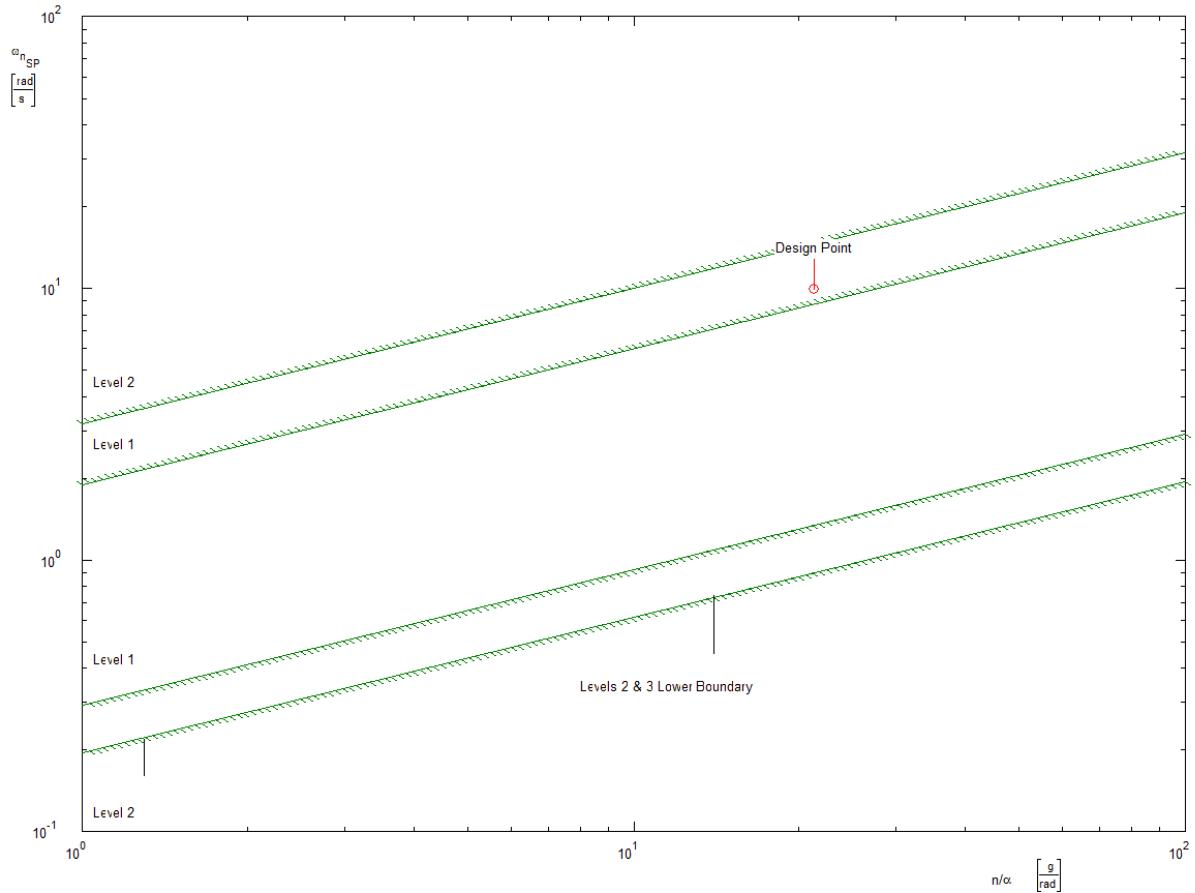


Fig. 11 Short period response is slightly outside level 1 requirements

AAA predicts that the Twin Sea Lion will have excellent flying qualities. AAA lists the relevant coefficients in Figure 87. In the phugoid mode, $\omega_P = 0.053s^{-1}$ and $\zeta_P = 0.093$. Short period has $\omega_{SP} = 9.92s^{-1}$ and $\zeta_{SP} = 0.581$. The detailed transfer functions are in Figures 8, 9, and 10.

With the exception of short period frequency, all the flying qualities of the Twin Sea Lion are considered Level 1, indicating that they are acceptable without further modification. Short period frequency is considered Level 2. This means that it can probably be corrected. The abnormally high short period frequency is consistent with the abnormally high static margin of the Twin Sea Lion. Future revisions can probably correct both issues simultaneously by redesigning

the horizontal stabilizer.

2. Lateral-Directional Flying Qualities

Notably, the Twin Sea Lion is stable in spiral and dutch roll modes. This is unusual as most aircraft are either stable in dutch roll or spiral, but the unusual weight configuration distribution of the Twin Sea Lion, along with substantial dihedral and a very large tail mean that it manages stability in both modes.

IX. Design Changes Needed to Meet Mission Requirements or Improve Mission Performance

A. Conclusions

The Twin Sea Lion has begun to embody its name quite well. It is large, heavy, and likely quite loud. While its handling qualities are predicted to be quite fair, they are not perfect and many parts of the plane are perhaps over specialized. It has fallen short of its original range and payload requirements in order to maintain high cruising altitude and top speed. Whether this is a fair tradeoff is a decision for the pilot or operator, but the designers think they may have missed the mark. Nevertheless, the Twin Sea Lion represents a unique set of capabilities based around speed and altitude not normally seen in the turboprop class.

B. Recommended Design Changes

Large design changes ought to be considered for the Twin Sea Lion. Chief among them is whether the performance targets are feasible with current technology. In an effort to fly far, fast, and high, the aircraft has mostly become wing and engine at the expense of cargo and payload space. By flying shorter missions, more weight could be moved towards cargo and passengers instead of fuel. By altitude requirements, the wings and control surface sizes could be reduced. Finally, takeoff altitude and speed requirements would allow for reductions to maximum engine power. In addition, reworking the horizontal stabilizer could reduce pitch stiffness and make the plane more flyable overall.

However, these are all substantial and require significant extra work. Smaller changes might include moving to composite construction. An all carbon fiber aircraft would have savings not only from reduced structural weight, but all the efficiencies that follow as fuel and powerplant requirements also decrease. That room could be used for cargo, stronger landing gear, and better high lift devices to maintain the original goals of STOL performance and long range. In addition, fewer rivets would decrease drag moderately.

In either case, the authors believe that the first changes should be made to the empennage. The high aspect ratios of the horizontal and vertical stabilizers make the aircraft excessively stiff in pitch and yaw and smaller surfaces would likely suffice. If the elevator and rudder authorities are insufficient, the elevators and rudders could be made into all-moving tailplanes in order to keep adequate area for the aerodynamic surfaces.

References

- [1] Junker and Killelea, "Design Report 01: Twin Sea Lion."
- [2] Junker and Killelea, "Design Report 02: Twin Sea Lion."
- [3] Junker and Killelea, "Design Report 03: Twin Sea Lion."
- [4] Gerren, "Handout #1", <https://canvas.colorado.edu>
- [5] Gerren, "Handout #2", <https://canvas.colorado.edu>
- [6] Gerren, "Handout #3", <https://canvas.colorado.edu>
- [7] Gerren, "Handout #4", <https://canvas.colorado.edu>
- [8] Gerren, "Presentation 26", <https://canvas.colorado.edu>
- [9] Gerren, "Presentation 27", <https://canvas.colorado.edu>

X. Appendix

A. AAA: Stability and Control Derivatives

Wing Lift Curve Slope: Flight Condition 1								
Input Parameters								
Altitude	30000 ft	$C_{L_0} @ M=0$	6.3598 rad ⁻¹	AR_{w}	8.00	$V_{\text{ref}}_{\text{w}}$	0.00 ft	$(\rho v_0^2 C_L)_0$
ΔT	0.0 deg F	$C_{L_0} @ M=0$	6.3598 rad ⁻¹	L_{ref}	0.60	$(\rho C_L)_{\text{ref}}$	12.00 %	$(\rho C_D)_{\text{ref}}$
U_1	350.00 m/s	S_0	837.00 m ²	$\Delta \alpha_{\text{ref}}$	0.0 deg	$(\rho C_L)_0$	12.00 %	D_{ref}
Output Parameters								
M_1	0.594	t_{ref}	0.93	C_{L_0}	7.9041 rad ⁻¹	S_{ref}	751.13 m ²	$C_{L_{\text{ref}}}$
K_{ref}	1.0003	$C_{L_0} @ M=0$	6.3598 rad ⁻¹	$C_{L_{\text{ref}}}$	7.9041 rad ⁻¹	AR_{ref}	7.49	$C_{L_{\text{ref}} @ M=0}$
t_{ref}	0.91	C_{L_0}	7.9041 rad ⁻¹	B_{ref}	75.00 ft	b_{ref}	0.62	$C_{L_{\text{ref}} @ M=0}$
High Lift Devices Table								
#	High Lift Device	η_i %	η_o %	ϵc_w %	δ deg			
1	Single Slotted Flap	9.0	55.5	30.0	0.0			

Fig. 12 Wing lift curve slope

Wing Lift Coefficient at Alpha = 0 deg: Flight Condition 1										
Input Parameters										
Altitude	30000 ft	S_0	837.00 ft^2	$\Delta_{\alpha_{\text{L}}}$	0.0 deg	$C_{\text{L}_{\text{ref},\text{clean}}}$	5.3724 rad ⁻¹	$\alpha_{\text{ref},\text{M=0}}$	6.3598 rad ⁻¹	
ΔT	0.0 deg F	AR_w	8.00	$C_{\text{L}_{\text{ref},\text{clean}}}$	5.3706 rad ⁻¹	$C_{\text{L}_{\text{ref}}}$	5.3724 rad ⁻¹	$\alpha_{\text{ref},\text{M=0}}$	-3.0 deg	
U_1	350.00 kts	τ_w	0.60	$C_{\text{L}_{\text{ref}}}$	5.3706 rad ⁻¹	$C_{\text{L}_{\text{ref},\text{M=0}}}$	6.3598 rad ⁻¹	$\alpha_{\text{ref},\text{M=0}}$	3.0 deg	
Output Parameters										
M_1	0.594	α_{ref}	0.0 deg	$C_{\text{L}_{\text{ref},\text{M=0}}}$	6.3598 rad ⁻¹	$\alpha_{\text{ref},\text{M=0}}$	-3.0 deg	$\Delta C_{\text{L}_{\text{ref},\text{M=0}}}$	0.0000	
$\alpha_{\text{ref},w}$	-3.0 deg	$\alpha_{\text{ref},w}$	7.9041 rad ⁻¹	$C_{\text{L}_{\text{ref}}}$	7.9041 rad ⁻¹	α_{ref}	-3.0 deg	$\Delta C_{\text{L}_{\text{ref}}}$	0.0000	
α_{ref}	-3.0 deg	$C_{\text{L}_{\text{ref}}}$	7.9041 rad ⁻¹	$\alpha_{\text{ref},w}$	-0.4	$\alpha_{\text{ref},\text{M=0}}$	2.0 deg	$C_{\text{L}_{\text{ref},\text{M=0}}}$	0.2812	
High Lift Devices Table										
#	High Lift Device	η_1 %	η_0 %	ηC_w %	β deg	ΔC_{w_0}				
1	Single Slotted Flap	9.0	55.5	30.0	0.0	0.0000				

Fig. 13 Wing lift coefficient at zero angle of attack

Horizontal Tail Lift Curve Slope: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	$\alpha_{\text{ref},\text{M=0}}$	6.2504 rad ⁻¹	AR_h	7.00	V_{dih_h}	0.00 ft	w_{t_0}	2.00 ft
ΔT	0.0 deg F	$\alpha_{\text{ref},\text{M=0}}$	6.2504 rad ⁻¹	τ_h	1.00	$(\eta C)_h$	12.0 %	$(\eta C)_{C_h}$	0.00 %
U_1	350.00 kts	S_0	190.00 ft^2	$\Delta_{\alpha_{\text{L}}}$	0.0 deg	$(\eta C)_h$	12.0 %	$(\eta C)_{\text{ref}}$	70.00 %
Output Parameters									
M_1	0.594	AR_{ref}	6.62	β_{ref}	34.47 ft	$C_{\text{L}_{\text{ref},\text{M=0}}}$	5.3097 rad ⁻¹	τ_{ref}	1.00
S_{ref}	179.58 ft^2	α_{ref}	1.00	$(\eta C)_{\text{ref}} + K_{\text{ref}}$	1.12	$\alpha_{\text{ref},\text{M=0}}$	1.00	$C_{\text{L}_{\text{ref},\text{M=0}}}$	6.2504 rad ⁻¹
						$\alpha_{\text{ref},\text{M=0}}$	7.7681 rad ⁻¹	α_{ref}	7.7681 rad ⁻¹

Fig. 14 Horizontal stabilizer lift curve slope

Horizontal Tail Downwash Gradient: Flight Condition 1									
Input Parameters									
S_0	837.00 ft^2	$\Delta_{\alpha_{\text{L}}}$	0.0 deg	Z_{ref}	2.00 ft	$C_{\text{L}_{\text{ref},\text{M=0}}}$	4.5851 rad ⁻¹	AR_h	7.00
AR_w	8.00	X_{ref}	23.00 ft	τ_w	-1.0 deg	$C_{\text{L}_{\text{ref}}}$	5.3706 rad ⁻¹	τ_h	1.00
τ_w	0.60	V_{dih_h}	0.00 ft	$C_{\text{L}_{\text{ref},\text{M=0}}}$	5.3706 rad ⁻¹	S_0	190.00 ft^2	λ_{ref}	0.0 deg
								V_{dih_h}	0.00 ft
Output Parameters									
Z_{ref}	6.00 ft	b_h	35.11 ft	$(\eta D)_{\text{ref}}$	0.4274	$(\eta D)_{\text{ref},\text{M=0}}$	0.4274	$(\eta D)_{\text{ref}}$	0.3931
								$(\eta D)_{\text{ref}}$	0.3931
								$(\eta D)_{\text{ref}}$	0.3931
High Lift Devices Table									
#	High Lift Device	η_1 %	η_0 %						
1	Single Slotted Flap	9.0	55.5						

Fig. 15 Horizontal stabilizer downwash gradient

Horizontal Tail Downwash Angle: Flight Condition 1					
Input Parameters					
$C_{l_{\alpha_{\text{clean}}}}$	5.3706 rad ⁻¹	$(ds/d\alpha)_{M=0}$	0.3356	δ_w	-1.0 deg
$C_{l_{\alpha_{\text{clean}}}} @ M=0$	4.5051 rad ⁻¹	α_{clean}	-3.0 deg	S_w	837.00 ft ²
$Z_{l_{\alpha_{\text{clean}}}}$		$Z_{l_{\alpha_{\text{clean}}}} @ M=0$	2.00 ft	AR_w	8.00
z_{ht}	6.00 ft				
Output Parameters					
$\Delta \delta_{l_{\alpha_{\text{HTD}}}}$	0.0 deg	$\delta_{l_{\alpha_{\text{HTD}}}} @ M=0$	0.7 deg	$\delta_{l_{\alpha_{\text{HTD}}}}$	0.8 deg
High Lift Devices Table					
#	High Lift Device	η_i %	η_0 %	$\Delta C_{L_{W_0}}$	
1	Single Slotted Flap	9.0	55.5	0.0000	

Fig. 16 Horizontal stabilizer downwash angle

Horizontal Tail Lift Coefficient at Zero Horizontal Tail Angle of Attack: Flight Condition 1					
Input Parameters					
Altitude	30000 ft	S_h	190.00 ft ²	$\Lambda_{c_{l_{\alpha_h}}}$	0.0 deg
ΔT	0.0 deg F	AR_h	7.00	$C_{l_{\alpha_{\text{HTD}}}} @ M=0$	6.2504 rad ⁻¹
U_1	350.00 kts	z_h	1.00	$\alpha_{\text{HTD}} @ M=0$	0.0 deg
ϵ_{T_h}				$(U/c)_h$	12.0 %
M_1	0.594	$C_{l_{\alpha_{\text{HTD}}}}$	7.7681 rad ⁻¹	α_{HTD}	0.0 deg
α_{e_m}	7.7681 rad ⁻¹	α_{e_h}	0.0 deg	ϵ_{T_h}	0.0 deg
$\alpha_{e_m} @ M=0$		$\alpha_{e_h} @ M=0$		α_{e_h}	0.0 deg
$C_{l_{\alpha_{\text{HTD}}}}$	0.0000				
Output Parameters					
M_1	0.594	$C_{l_{\alpha_{\text{HTD}}}}$	7.7681 rad ⁻¹	α_{HTD}	0.0 deg
α_{e_m}	7.7681 rad ⁻¹	α_{e_h}	0.0 deg	ϵ_{T_h}	0.0 deg
$\alpha_{e_m} @ M=0$		$\alpha_{e_h} @ M=0$		α_{e_h}	0.0 deg
$(U/c)_h$	12.0 %				

Fig. 17 Horizontal stabilizer lift coefficient at zero angle of attack

Vertical Tail Sidewash Gradient: Flight Condition 1					
Input Parameters					
S_w	837.00 ft ²	$\Lambda_{c_{l_{\alpha_v}}}$	0.0 deg	$Z_{l_{\alpha_v}}$	2.50 ft
AR_w	8.00	$Z_{l_{\alpha_v}} @ M=0$	2.00 ft	h_w	2.50 ft
z_{ht}				S_v	137.00 ft ²
Output Parameter					
$(d\alpha/d\beta)_v$	-0.1264				

Fig. 18 Vertical stabilizer sidewash gradient

Vertical Tail Downwash Gradient: Flight Condition 1																																							
Input Parameters																																							
S_w	<input type="text" value="837.00"/> ft ²	ΔC_{L_w}	<input type="text" value="0.0"/> deg	Z_{c/L_w}	<input type="text" value="2.00"/> ft	$C_{L_{w_0} @ M=0}_{\text{clean}}$	<input text"="" type="text" value="8.00"/>	X_{emp_w}	<input type="text" value="23.00"/> ft	i_w	<input type="text" value="-1.0"/> deg	$C_{L_{w_0}}$	<input text"="" type="text" value="0.60"/>	Y_{chord_w}	<input type="text" value="0.00"/> ft	$C_{L_{w_0} \text{ clean}}$	<input 1"="" text"="" type="text" value="15.00} ft</td> </tr> </tbody> </table>
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1	Single Slotted Flap	<input type="text" value="9.0"/>	<input type="text" value="55.5"/>																																				

Fig. 19 Vertical stabilizer downwash gradient

Vertical Tail Downwash Angle: Flight Condition 1																							
Input Parameters																							
$C_{L_{w_0} \text{ clean}}$	<input 1"="" text"="" type="text" value="837.00} ft<sup>2</sup></td> </tr> <tr> <td><math>Z_{w_v}</math></td> <td></td> <td><math>Z_{c/L_w}</math></td> <td></td> <td></td> <td></td> </tr> </tbody> </table>
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High Lift Devices Table																							
#	High Lift Device	η_l %	η_o %																				
1	Single Slotted Flap	<input type="text" value="9.0"/>	<input type="text" value="55.5"/>																				
		$\Delta C_{L_{w_0}}$	<input 342="" 516="" 532"="" 652="" data-label="Caption" type="text" value="0.0000} deg</td> </tr> </tbody> </table> </div> <div data-bbox="/> <p>Fig. 20 Vertical stabilizer downwash angle</p>																				

Wing Lift Coefficient for Given Angle of Attack: Linear Range: Flight Condition 1									
Input Parameters									
α	<input 1"="" text"="" type="text" value="5.3724} rad<sup>-1</sup></td> </tr> </tbody> </table>
 <table border="/> <thead> <tr> <th colspan="6">Output Parameters</th> </tr> </thead> <tbody> <tr> <td>α_{off}</td> <td><input 394="" 601="" 725="" 741"="" data-label="Caption" text"="" type="text" value="0.0000}</td> </tr> </tbody> </table> </div> <div data-bbox="/> <p>Fig. 21 Wing lift coefficient</p> </td></tr></tbody>	Output Parameters						α_{off}	<input 394="" 601="" 725="" 741"="" data-label="Caption" text"="" type="text" value="0.0000}</td> </tr> </tbody> </table> </div> <div data-bbox="/> <p>Fig. 21 Wing lift coefficient</p>
Output Parameters									
α_{off}	<input 394="" 601="" 725="" 741"="" data-label="Caption" text"="" type="text" value="0.0000}</td> </tr> </tbody> </table> </div> <div data-bbox="/> <p>Fig. 21 Wing lift coefficient</p>								

Subsonic Wing Drag Coefficient Prediction: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	S _w	837.00 ft ²	A _{lif} S _w	1.8 deg	(R ₀ /C) _w	1.000 %	L _w	1.2
ΔT	0.0 deg F	AR _w	8.00	(U/C) _w	12.00 %	S _{ref,w}	837.00 ft ²	(X _{ref} /C) _w	15.0 %
U ₁	350.00 kts	I _w	0.60	k _{cord}	0.01333 10 ⁻³ ft	C _{D,app}	10.20 ft	C _{D,w}	7.9041 rad ⁻¹
C _{D,w}	0.1875	Δα _{CD,w}	0.0 deg	C _{D,app}	10.44 ft	I _w	55.00 ft	C _{D,app}	5.3706 rad ⁻¹
Output Parameters									
M ₁	0.594	Re _{num}	0.2590 × 10 ⁶	C _w	0.0024	C _{D,app,ref}	0.00020	C _{D,w}	0.0015
Re _{x,ref}	1.4677 × 10 ⁶	Re _{x,cal}	5.3833 × 10 ⁶	ε _w	0.9514	C _{D,app}	0.0037		
High Lift Devices Table									
#	High Lift Device	C _{D,gap}							
1	Single Slotted Flap	0.00020							

Fig. 22 Wing drag coefficients

Wing Aerodynamic Center: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	U ₁	350.00 kts	AR _w	8.00	A _{lif} S _w	0.0 deg	Y _{stab,w}	0.00 ft
ΔT	0.0 deg F	S _w	837.00 ft ²	I _w	0.60	X _{app,w}	23.00 ft	Z _{z,stab,w}	2.00 ft
Output Parameters									
M ₁	0.594	I _w	10.44 ft	Y _{app,w}	18.75 ft	X _w	26.20 ft	Z _w	0.2500
Q _t	155.41 ft ² /s ²	X _{app,w}	0.59 ft	X _w /C _w	0.2500	Z _w	3.64 ft		

Fig. 23 Wing aerodynamic center

Horizontal Tail Aerodynamic Center: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	U ₁	350.00 kts	AR _t	7.00	A _{lif} S _t	0.0 deg	Y _{stab,t}	0.00 ft
ΔT	0.0 deg F	S _t	190.00 ft ²	I _t	1.00	X _{app,t}	60.00 ft	Z _{z,stab,t}	6.00 ft
Output Parameters									
M ₁	0.594	I _t	155.41 ft ² /s ²	C _t	5.21 ft	X _{app,t}	0.00 ft	Y _{app,t}	9.12 ft
								X _t	61.30 ft
								Z _t	6.00 ft

Fig. 24 Horizontal stabilizer aerodynamic center

Vertical Tail Aerodynamic Center: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	U ₁	350.00 kts	AR _t	3.00	A _{lif} S _t	5.0 deg	Z _{app,t}	15.00 ft
ΔT	0.0 deg F	S _t	137.00 ft ²	I _t	0.80	X _{app,t}	60.00 ft		
Output Parameters									
M ₁	0.594	I _t	155.41 ft ² /s ²	C _t	6.79 ft	X _{app,t}	1.03 ft	Z _{app,t}	9.76 ft
								X _t	62.73 ft
								Z _t	24.76 ft

Fig. 25 Vertical stabilizer aerodynamic center

Calculation of the Aerodynamic Center Shift due to Fuselage: Flight Condition 1											
Input Parameters											
S_w	837.00	ft^2	b_{ref}	0.60	$X_{\text{ref}}_{\text{w}}$	23.00	ft	$C_{L_{\text{ref}} \text{ @ } M=0}$	4.5851	rad^{-1}	
ARe	8.00		$\Delta c_{L_{\text{ref}}}$	0.0	$V_{\text{ref}}_{\text{w}}$	0.00	ft	$C_{L_{\text{ref}} \text{ @ } M=0}$	5.3724	rad^{-1}	
								k	55.00	ft	
								N_b	8		
Output Parameters											
$X_{\text{ref}}_{\text{w}}$	0.59	ft	$C_{L_{\text{ref}}}$	10.44	ft	$C_{L_{\text{ref}}}$	12.36	ft	b_{ref}	23.11	ft
								b_{ref}	19.53	ft	
								$\Delta C_{L_{\text{ref}}}$	-0.0451		
Fuselage Table											
Section	X_{fus}_1	ft	A_{fus}_1	ft^2							
1	0.0000	0.00									
2	4.5000	19.60									
3	15.0000	36.30									
4	47.0000	36.30									
5	55.0000	9.18									
6	60.0000	3.14									
7	66.0000	3.14									
8	66.1000	0.00									

Fig. 26 Aerodynamic center shift due to fuselage effects

Power-off Dynamic Pressure Ratio: Flight Condition 1										
Input Parameters										
α	0.00	deg	b_{ref}	0.6	deg	ARe	8.00	b_{ref}	-1.0	deg
a_{b_0}	0.8	deg	$(\partial b_0 / \partial X)_{p,\text{off}}$	0.2787		b_{ref}	0.60	$Z_{\text{ref}}_{\text{w}}$	2.00	ft
								$Z_{\text{ref}}_{\text{w}}$	6.00	ft
								N_b	2	
$(\partial b_0 / \partial X)_{p,\text{off}}$	0.3931		S_w	837.00	ft^2	$X_{\text{ref}}_{\text{w}}$	23.00	$C_{L_{\text{ref}} \text{ @ } M=0}$	0.0037	
								$X_{\text{ref}}_{\text{w}}$	62.73	ft
								α_{off}	-5.0	deg
Output Parameters										
C_L	10.44	ft	$\Delta Z_{\text{ref}}_{\text{w}}$	0.70	ft	b_{ref}	1.000	$\Delta Z_{\text{ref}}_{\text{w}}$	0.71	ft
$Z_{\text{ref}}_{\text{w}}$	4.18	ft	b_{ref}	1.000		$Z_{\text{ref}}_{\text{w}}$	22.85	b_{ref}	1.000	

Fig. 27 Power-off dynamic pressure ratio

Elevator Related Derivatives: Flight Condition 1										
Input Parameters										
Altitude	30000	ft	$C_{L_{\text{e}} \text{ @ } M=0}$	6.2504	rad^{-1}	b_{ref}	1.00	$b/C_{L_{\text{e}}}$	12.0	%
ΔT	0.0	deg F	$C_{L_{\text{e}} \text{ @ } M=0}$	6.2504	rad^{-1}	$\Delta c_{L_{\text{e}}}$	0.0	deg	5.7070	rad^{-1}
U_1	350.00	kts	S_w	190.00	ft^2	m_{ref}	1.000	$c_e/C_{L_{\text{e}}}$	28.5	%
S_w	837.00	ft^2	ARe	7.00		$(\partial C_{L_{\text{e}}} / \partial \alpha)$	12.0	%	$(\partial C_{L_{\text{e}}} / \partial \alpha)$	0.00
						b_{ref}	5.0	%	b_{ref}	0.05
						$\text{Balance}_{\text{e}}$			$(C_e/C_{L_{\text{e}}})_{\text{max}}$	
Output Parameters										
M_1	0.594		$C_{L_{\text{e}}}$	7.7681	rad^{-1}	V_{ref}	1.0000	$C_{L_{\text{e}}}$	0.4231	
$C_{L_{\text{e}}}$	7.7681	rad^{-1}	$C_{L_{\text{e}}}$	1.2955	rad^{-1}	b_{ref}	1.00	$C_{L_{\text{e}}}$	2.4149	rad^{-1}
								b_{ref}	0.4231	
								$C_{L_{\text{e}}}$	-0.0003	

Fig. 28 Elevator related derivatives

Horizontal Tail Lift Coefficient for Given Angle of Attack: Linear Range: Flight Condition 1											
Input Parameters											
α	0.00	deg	$(\partial b_0 / \partial X)_{p,\text{off}}$	0.3931		a_{b_0}	0.0	deg	$C_{L_{\text{h}} \text{ @ } M=0}$	2.4149	rad^{-1}
a_{b_0}	0.8	deg	b	0.0	deg	$C_{L_{\text{h}}}$	5.7070	rad^{-1}	$c_e/C_{L_{\text{e}}}$	28.5	%
								$\eta_{\text{h},\text{off}}$	1.000		
Output Parameters											
X_{h}	1.0000		z_{h}	0.79	deg	a_{b_0}	-0.8	deg	$C_{L_{\text{h}}}$	-0.0798	

Fig. 29 Horizontal tail lift coefficient

Steady State Coefficients: Lift Flight Condition 1																			
Input Parameters																			
Altitude	30000 ft	$W_{airmass}$	37689.0 lb	S_w	837.00 ft^2	$D_{w_{\text{ref}}}$	-3.0 deg	I_w	0.60										
ΔT	0.0 deg F	i_w	1.00 deg	γ	0.0 deg	AR_w	8.00	A_{ref}	0.0 deg										
U_1	350.00 kts	α	0.00 deg	β_w	-1.0 deg	V_{ref, α_w}	0.00 n	X_{ref, α_w}	23.00 n										
								$C_{L_w @ \alpha=0, \text{Clean}}$	4.5851 rad^{-1}										
Output Parameters																			
M_1	0.594	ZSH_{ref}	3109 hp	λ_{ref, α_w}		θ_{T_1}	7.0 deg	C_{L_1}	0.1076										
Q_1	155.41 $\frac{\text{lb}}{\text{s}}$	ZP_{ref}	2492 hp	ZT_{ref}	2320 lb	C_{L_1}	0.0022												
Propeller Table																			
#	Type	X_{prop} ft	Y_{prop} ft	Z_{prop} ft	D_{prop} ft	η_{prop} deg	$\delta_{0.75, \text{prop}}$ deg	$N_{\text{blades, p}}$	$(W/R)_{0.3R, \text{prop}}$	$(W/R)_{0.6R, \text{prop}}$	$(W/R)_{0.9R, \text{prop}}$	RHP_{set} hp	η_{prop}	$K_{\text{loss, \%}}$	P_{avail} hp	$T_{\text{cl, prop}}$	$\sigma_{\text{v/d}}$	$C_{N_{\text{prop}}}$	
1	Propeller: On	Input	Input	Input	Input	Input	Input	Input	Input	Input	Input	Input	Input	Input	Output	Output	Output	Output	
1	Propeller: On	22.00	9.01	4.00	9.25	7.0		5					1555	0.850	5.7	1246	0.0089	0.0000	0.0000
2	Propeller: On	22.00	-9.01	4.00	9.25	7.0		5					0	0.850	5.7	0	0.0000	0.0000	0.0000

Fig. 30 Steady state lift coefficients

Angle of Attack Related Derivatives: Lift Flight Condition 1									
Input Parameters									
Altitude	30000 ft	$t_{\rho_{w_{\text{ref}}}}$	0.93	i_w	-1.0 deg	$Z_{\alpha_{w_{\text{ref}}}}$	2.00 n	$X_{\alpha_{w_{\text{ref}}}}$	60.00 n
ΔT	0.0 deg F	S_w	837.00 ft^2	$X_{\alpha_{w_{\text{ref}}}}$	23.00 n	S_w	190.00 ft^2	$V_{\alpha_{w_{\text{ref}}}}$	0.00 n
U_1	350.00 kts	AR_w	8.00	$V_{\alpha_{w_{\text{ref}}}}$	0.00 n	AR_w	7.00	$(\partial C_L)/(\partial \alpha)$	12.0 %
$C_{L_w @ M=0}$	6.3598 rad^{-1}	$\lambda_{w_{\text{ref}}}$	0.60	$(\partial C_L)/\alpha$	12.00 %	λ_w	1.00	$(\partial C_L)/\alpha$	12.0 %
$C_{L_w @ M=0}$	6.3598 rad^{-1}	$\lambda_{w_{\text{ref}}}$	0.00 deg	$(\partial C_L)/\alpha$	12.00 %	$Z_{\alpha_{w_{\text{ref}}}}$	0.00 deg	$Z_{\alpha_{w_{\text{ref}}}}$	6.00 n
Output Parameters									
M_1	0.594	$\lambda_{w_{\text{ref}}}$	7.9041 rad^{-1}	$C_{L_{w_{\text{ref}}}}$	5.3724 rad^{-1}	$\lambda_{w_{\text{ref}}}$	7.7681 rad^{-1}	$d\lambda/d\alpha$	0.3931
Q_1	155.41 $\frac{\text{lb}}{\text{s}}$	$C_{L_{w_{\text{ref}}}}$	5.3706 rad^{-1}	$K_{w_{\text{ref}}}$	1.0003	$Z_{w_{\text{ref}}}$	6.00 n	$C_{L_{w_{\text{ref}}}}$	5.7070 rad^{-1}
$C_{L_{w_{\text{ref}}}}$	7.9041 rad^{-1}	$C_{L_{w_{\text{ref}}}}$	5.3724 rad^{-1}	$\lambda_{w_{\text{ref}}}$	7.7681 rad^{-1}	$d\lambda/d\alpha$	0.3931	$C_{L_{w_{\text{ref}}}}$	0.7862 rad^{-1}
$C_{L_{w_{\text{ref}}}}$	7.9041 rad^{-1}	$C_{L_{w_{\text{ref}}}}$	5.3706 rad^{-1}	$\lambda_{w_{\text{ref}}}$	7.7681 rad^{-1}	$d\lambda/d\alpha$	0.3931	$C_{L_{w_{\text{ref}}}}$	5.3724 rad^{-1}
High Lift Devices Table									
#	High Lift Device	η_1 %	η_0 %	ηL_w %	β deg				
1	Single Slotted Flap	9.0	55.5	30.0	0.0				

Fig. 31 Angle of attack related derivatives

Airplane Aerodynamic Center: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	AR_w	8.00	$X_{\alpha_{w_{\text{ref}}}}$	23.00 n	$\lambda_{w_{\text{ref}}}$	61.30 n	S_w	190.00 ft^2
ΔT	0.0 deg F	i_w	0.60	$X_{w_{\text{ref}}}$	26.20 n	$C_{L_{w_{\text{ref}}}}$	5.7070 rad^{-1}	$X_{\alpha_{w_{\text{ref}}}}$	60.00 n
U_1	350.00 kts	$\lambda_{w_{\text{ref}}}$	0.0 deg	$C_{L_{w_{\text{ref}}}}$	5.3724 rad^{-1}	$(d\lambda/d\alpha)_{w_{\text{ref}}}$	0.3931	$\lambda_{w_{\text{ref}}}$	-0.0451
S_w	837.00 ft^2	i_w	-1.0 deg	$C_{L_{w_{\text{ref}}}}$	6.1586 rad^{-1}	$\eta_{w_{\text{ref}}}$	1.000	$X_{\alpha_{w_{\text{ref}}}}$	24.80 n
Output Parameters									
M_1	0.594	$\lambda_{w_{\text{ref}}}$	10.44 n	$\lambda_{w_{\text{ref}}}$	0.2500	$\lambda_{w_{\text{ref}}}$	0.2049	$X_{w_{\text{ref}}}$	25.73 n
Q_1	155.41 $\frac{\text{lb}}{\text{s}}$	$X_{w_{\text{ref}}}$	0.59 n	$X_{w_{\text{ref}}}$	0.2049	$X_{w_{\text{ref}}}$	25.73 n	$X_{w_{\text{ref}}}$	3.6121
								$\lambda_{w_{\text{ref}}}$	0.6399

Fig. 32 Aircraft aerodynamic center

Steady State Coefficients: Lift: Flight Condition 1																			
Input Parameters																			
Altitude	30000 ft	W_{fwd}	37689.0 lb	S_a	837.00 ft^2	D_{a_0}	-3.0 deg	i_w	0.60	$Z_{c_{L_1}}$	2.00 \pm								
ΔT	0.0 deg F	α	1.00 deg	γ	0.0 deg	AR_w	8.00	A_{ref}	0.0 deg	$C_{L_{\alpha, clean}}$	5.3706 rad^{-1}								
U_1	350.00 kts	α	0.00 deg	i_w	-1.0 deg	V_{atmos}	0.00 m	X_{atmos}	23.00 m	$C_{L_{\alpha, @m=0, clean}}$	4.5851 rad^{-1}								
Output Parameters																			
M_1	0.594	ΣSHP_{set}	3109 hp	$\Sigma C_{D_{prop}}$		$\phi_{T_{prop}}$	7.0 deg	C_{L_1}	0.1076										
\bar{q}_1	155.41 $\frac{\text{lb}}{\text{ft}^2}$	ΣP_{avail}	2492 hp	ΣT_{avail}	2320 lb	$C_{T_{x_1}}$	0.0022												
Propeller Table																			
#	Type	X_{prop} ft	Y_{prop} ft	Z_{prop} ft	D_{prop} ft	η_{prop} deg	$\delta_{0.75_{prop}}$ deg	N_{blades_p}	$(W/R)_{0.3R_{prop}}$	$(W/R)_{0.6R_{prop}}$	$(W/R)_{0.9R_{prop}}$	SHP_{set} hp	η_{prop}	$K_{loss} \%$	P_{avail} hp	$T_{c/prop}$	$\theta_{v/d}$	$C_{N_{prop}}$	
1	Propeller: On	22.00	9.01	4.00	9.25	7.0		5					1555	0.850	5.7	1246	0.0089	0.0000	0.0000
2	Propeller: On	22.00	9.01	4.00	9.25	7.0		5					0	0.850	5.7	0	0.0000	0.0000	0.0000

Fig. 33 Steady state lift coefficient

Steady State Coefficients: Drag: Flight Condition 1																
Input Parameters																
C_{L_1}	0.1076	\bar{C}_{D_1}		$B_{C_{D_1}}$		$B_{C_{D_2}}$		$B_{C_{D_3}}$		$B_{C_{D_4}}$		$B_{C_{D_5}}$		$B_{C_{D_6}}$		
Output Parameters																
C_{D_1}	0.0177	L_D	6.08													

Fig. 34 Steady state flight coefficients

Class I Current Flight Condition Drag Polar: Flight Condition 1											
Input Parameters											
W_{fwd}	37689.0 lb	AR_w	8.00	a	-2.3010	c	-0.0866	ΔC_{D_0}	0.0005	$C_{plot_{max}}$	3.0000
S_a	837.00 ft^2	i_w	0.60	b	1.0000	d	0.8099	$C_{plot_{min}}$	0.0000		
Output Parameters											
e	0.8560	f	20.83 ft^2	$\bar{C}_{D_{min}}$	0.0254	B_{D_P}	0.0465	$C_{L@C_{D_{min}}}$	0.0000		
S_{ref}	4165.58 ft^2	$\bar{C}_{D_{clean}}$	0.0249	A_{D_P}	0.0000	$C_{D_{min}}$	0.0254				

Fig. 35 Steady state drag polar calculations

Steady State Coefficient due to Thrust in X-direction: Flight Condition 1										
Input Parameters										
Altitude	30000 ft	ΔT	0.0 deg F	U_1	350.00 kts	α	0.00 deg	S_a	837.00 ft^2	
Output Parameters										
M_1	0.594	$\Phi_{T_{z,prop}}$	7.0 deg	ΣP_{avail}	2492 hp	Φ_{T_T}	7.0 deg			
\bar{q}_1	155.41 $\frac{\text{lb}}{\text{ft}^2}$	ΣSHP_{set}	3109 hp	ΣT_{avail}	2320 lb	$C_{T_{x_1}}$	0.0177			
Propeller Table										
#	Type	SHP_{set} hp	η_{prop}	i_{prop} deg	ψ_{prop} deg	$K_{loss} \%$	P_{avail} hp	T_{avail} lb	$T_{c/prop}$	$C_{T_{x_1}}$
1	Propeller: On	1555	0.850	7.0	0.0	5.7	1246	1160	0.0089	0.0089
2	Propeller: On	0	0.850	7.0	0.0	5.7	0	0	0.0000	0.0089

Fig. 36 Steady state thrust

Steady State Pitching Moment Coefficient due to Thrust: Flight Condition 1																		
Input Parameters																		
Altitude	30000 ft	U_1	350.00 kts	Z_{cg}	2.95 ft	AR_{fa}	8.00	α	0.00 deg									
ΔT	0.0 deg F	λ_{cg}	24.32	S_w	837.00 ft^2	b_w	0.60	a_{α_w}	-3.0 deg									
Output Parameters																		
M_1	0.594	C_{D_u}	10.44	D_{prop}	2492 hp	$\partial C_{L_{prop}}$	-0.0013	d_{CT}	0.76 ft									
q_1	155.41 lb/ft ²	$D_{SHP_{net}}$	3109 hp	$\lambda D_{L_{prop}}$	0.0000	$D_{T_{net}}$	2320 lb	d_{C_N}	2.43 ft									
Propeller Table																		
#	X _{prop} ft	Z _{prop} ft	D _{prop} ft	i _{prop} deg	ψ_{prop} deg	C _{N_{prop}} rad	I _{inflow}	$\frac{dC}{d\alpha}$	SHP set hp	% _{prop}	C _{D_{prop}wm}	C _{D_{prop}stop}	K _{loss} %	d _T ft	d _N ft	P _{avail} hp	T _{c_{prop}}	
1	Type	Input	Input	Input	Input	Input	Input	Input	Input	Input	Input	Input	Input	Output	Output	Output	Output	
1	Propeller: On	22.00	4.00	9.25	7.0	0.0	0.0000	1.0402	0.0000	1555	0.850	0.0000	0.0000	5.7	0.76	2.43	1246	0.0089
2	Propeller: On	22.00	4.00	9.25	7.0	0.0	0.0000	1.0402	0.0000	0	0.850	0.0000	0.0000	5.7	0.76	2.43	0	0.0000

Fig. 37 Steady state pitching moment

State Coefficients: Pitching Moment: Flight Condition 1

Output Parameter

C_{mr_1}	0.0013
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Fig. 38 Steady state pitching moment

Speed Related Derivatives: Drag: Flight Condition 1				
Input Parameters				
Altitude	30000 ft	ΔT	0.0 deg F	U_1
	30000 ft	0.0 deg F	350.00 kts	$\partial C_D/\partial M$
Output Parameters				
M_1	0.594	C_{D_u}	0.0000	

Fig. 39 Speed related derivatives

Speed Related Derivatives: Lift: Flight Condition 1					
Input Parameters					
Altitude	30000 ft	ΔT	0.0 deg F	U_1	350.00 kts
	30000 ft	0.0 deg F	350.00 kts	C_{L_1}	0.1076
Output Parameters					
M_1	0.594	q_1	155.41 lb/ft ²	C_{L_u}	0.0586

Fig. 40 Speed related derivatives

Speed Related Derivatives: Pitching Moment: Flight Condition 1													
Input Parameters													
Altitude	30000 ft	$C_{L_{\alpha_{\text{ref}}(M=0)}}$	6.3598 rad ⁻¹	Δ_{roll_w}	0.0 deg	$(\partial C_L)_w$	12.00 %	$X_{\text{cg}_{\text{ref}}}$	60.00 ft	τ_w	0.0 deg	$I_{x_{\text{cg}}}$	1.00
ΔT	0.0 deg F	I_{roll_w}	0.93	$X_{\text{cg}_{\text{ref}}}$	23.00 ft	S_b	190.00 ft ²	$Y_{\text{cg}_{\text{ref}}}$	0.00 ft	n_{roll}	1.000	w_b	2.00 ft
U_1	350.00 kts	S_a	837.00 ft ²	$Y_{\text{cg}_{\text{ref}}}$	0.00 ft	AR_b	7.00	$(\partial C)_b$	12.0 %	n_b	1.000	D_{roll}	6.83
$C_{l_{\text{ref}}}$	0.1076	AR_w	8.00	Z_{roll_w}	2.00 ft	b_b	1.00	$(\partial C)_b$	12.0 %	$C_{\text{roll}_{\text{ref}}(M=0)}$	6.2504 rad ⁻¹	ΔC_{roll}	-0.0451
$C_{\text{roll}_{\text{ref}}(M=0)}$	6.3598 rad ⁻¹	β_w	0.60	$(\partial C)_w$	12.00 %	Δ_{roll_b}	0.0 deg	Z_{roll_b}	6.00 ft	$C_{\text{roll}_{\text{ref}}(M=0)}$	6.2504 rad ⁻¹		
Output Parameters													
M_1	0.594	$C_{L_{\alpha_{\text{ref}}}}$	5.2621 rad ⁻¹	$\delta_{\text{roll}}(M)$	-0.1666	C_{roll_b}	7.7681 rad ⁻¹	C_{roll_b}	5.7070 rad ⁻¹	\bar{Z}_{roll}	0.6399		
C_{roll_b}	7.9041 rad ⁻¹	C_{roll_b}	5.3706 rad ⁻¹	X_{cg_w}	26.20 ft	C_{roll_b}	7.7681 rad ⁻¹	C_{roll_b}	0.7062 rad ⁻¹	\bar{q}_1	155.41		
C_{roll_b}	7.9041 rad ⁻¹	C_{roll_b}	5.3724 rad ⁻¹	Z_{roll_w}	0.2500	C_{roll_b}	7.7681 rad ⁻¹	X_{cg_b}	61.30 ft	\bar{Z}_{roll}	10.44		
C_{roll_b}	7.9041 rad ⁻¹	X_{cg_w}	0.59 ft	Z_{roll_w}	0.2049	C_{roll_w}	5.3097 rad ⁻¹	Z_{roll_b}	3.6121	C_{roll_b}	0.0106		
High Lift Devices Table													
#	High Lift Device	η_1 %	η_0 %	$C_{L_{\alpha}} \eta$ %	β deg								
1	Single Slotted Flap	9.0	55.5	30.0	0.0								

Fig. 41 Speed related derivatives

Speed Related Derivatives: Thrust: Flight Condition 1

Input Parameter

C_{T_x}	0.0177
-----------	---------------

Output Parameter

$C_{T_x_u}$	-0.0531
-------------	----------------

Propeller Table

		C_{T_x}	$C_{T_x_u}$
#	Type	Input	Output
1	Propeller: On	0.0089	-0.0266
2	Propeller: On	0.0089	-0.0266

Fig. 42 Speed related derivatives

Speed Related Derivatives: Pitching Moment due to Thrust: Flight Condition 1									
Input Parameters									
S_w	837.00 ft ²	AR_w	8.00	J_w	0.60	X_cg	24.32 ft	Z_cg	2.95 ft
Output Parameters									
$d\zeta_T$	0.76 ft	Φ_T	7.0 deg	$d\zeta_N$	2.43 ft	\bar{C}_w	10.44 ft		
$d\zeta_N$	2.43 ft	$d\zeta_T$	0.76 ft	Φ_T	7.0 deg	C_{m_T}	0.0038		
Propeller Table									
		X_{prop} ft	Z_{prop} ft	i_{prop} deg	C_{T_x}	C_{m_T}			
#	Type	Input	Input	Input	Input	Output			
1	Propeller: On	22.00	4.00	7.0	-0.0266	0.0019			
2	Propeller: On	22.00	4.00	7.0	-0.0266	0.0019			

Fig. 43 Speed related derivatives

Angle of Attack Related Derivatives: Drag: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	M_1	0.594	$\bar{C}_{D_{\alpha}}$	0.0254	B_{DP}	0.0465	$C_{L_{DP,off}}$	6.1586 rad ⁻¹
ΔT	0.0 deg F	α	0.00 deg	A_{DP}	0.0000	$C_{L_{DP,off}}$	0.1698		
Output Parameter									
$C_{D_{\alpha}}$	0.0972 rad ⁻¹								

Fig. 44 Angle of attack related derivatives

Angle of Attack Related Derivatives: Lift: Flight Condition 1													
Input Parameters													
Altitude	30000 ft	t_{ref_w}	0.93	$\bar{\alpha}$	-1.0 deg	Z_{ref_w}	2.00 ft	X_{ref_w}	60.00 ft	Γ_w	2.00 ft		
ΔT	0.0 deg F	S_0	837.00 ft ²	X_{ref_w}	23.00 ft	S_0	190.00 ft ²	V_{ref_w}	0.00 ft	n_{ref}	1.000	D_{ref_w}	5.83 ft
U_1	350.00 ft/s	AR_w	8.00	$(\bar{C}_L)_w$	0.00 %	AR_b	7.00	$(\bar{C}_L)_b$	12.0 %	$C_{L_{ref,off}}$	6.2504 rad ⁻¹		
$C_{L_{ref,off}}$	6.3598 rad ⁻¹	$\bar{\alpha}_w$	0.60	$(\bar{C}_L)_w$	12.00 %	$\bar{\alpha}_b$	1.00	$(\bar{C}_L)_b$	12.0 %	$C_{L_b,off}$	6.2504 rad ⁻¹		
$C_{L_{ref,off}}$	6.3598 rad ⁻¹	$\Delta \bar{\alpha}_w$	0.0	$(\bar{C}_L)_w$	12.00 %	$\Delta \bar{\alpha}_b$	0.0	Z_{ref_b}	6.00 ft	Γ_w	1.00		
Output Parameters													
M_1	0.594	C_{L_w}	7.9041 rad ⁻¹	$C_{L_{ref}}$	5.3724 rad ⁻¹	C_{L_b}	7.7681 rad ⁻¹	$dL/d\alpha$	0.3931	$C_{L_{ref,clean}}$	5.3724 rad ⁻¹	C_b	6.1586 rad ⁻¹
$\bar{\alpha}$	155.41	$C_{L_w,off}$	5.3706 rad ⁻¹	$C_{L_{ref,off}}$	1.0003	Z_{ref_b}	6.00 ft	C_{L_w}	5.7070 rad ⁻¹	$C_{L_{ref,clean,off}}$	6.1586 rad ⁻¹		
$C_{L_{ref}}$	7.9041 rad ⁻¹	$C_{L_{ref,clean}}$	5.3724 rad ⁻¹	$C_{L_{ref,off}}$	7.7681 rad ⁻¹	$dL/d\alpha_{off}$	0.3931	C_{L_b}	0.7962 rad ⁻¹	$C_{L_{ref,off}}$	6.1586 rad ⁻¹		
C_{L_w}	7.9041 rad ⁻¹	C_{L_w}	5.3706 rad ⁻¹	C_{L_b}	7.7681 rad ⁻¹	$dL/d\alpha_{off}$	0.3931	$C_{L_{ref,clean}}$	5.3724 rad ⁻¹	$C_{L_{ref}}$	6.1586 rad ⁻¹		
High Lift Devices Table													
#	High Lift Device	$\bar{\alpha}_1$ %	$\bar{\alpha}_0$ %	$d\bar{\alpha}_w$ %	$\bar{\alpha}$ deg								
1	Single Slotted Flap	9.0	55.5	30.0	0.0								

Fig. 45 Angle of attack related derivatives

Angle of Attack Related Derivatives: Pitching Moment: Flight Condition 1													
Input Parameters													
Altitude	30000 ft	t_{ref_w}	0.93	X_{ref_w}	23.00 ft	S_0	190.00 ft ²	V_{ref_w}	0.00 ft	n_{ref}	1.000	D_{ref_w}	5.83 ft
ΔT	0.0 deg F	S_0	837.00 ft ²	V_{ref_w}	0.00 ft	AR_b	7.00	$(\bar{C}_M)_w$	12.0 %	$C_{M_{ref,off}}$	6.2504 rad ⁻¹	ΔX_{ref}	0.0451
U_1	350.00 ft/s	AR_w	8.00	$(\bar{C}_M)_w$	12.00 %	$\bar{\alpha}_b$	1.00	$(\bar{C}_M)_b$	12.0 %	$C_{M_b,off}$	6.2504 rad ⁻¹	X_M	24.32 ft
$C_{M_{ref,off}}$	6.3598 rad ⁻¹	$\bar{\alpha}_w$	0.60	$(\bar{C}_M)_w$	12.00 %	$\bar{\alpha}_b$	0.0	Z_{ref_b}	6.00 ft	Γ_w	1.00		
$C_{M_{ref,off}}$	6.3598 rad ⁻¹	$\Delta \bar{\alpha}_w$	0.0	Z_{ref_w}	2.00 ft	X_{ref_w}	60.00 ft	Γ_b	0.0 deg	w_b	2.00 ft		
Output Parameters													
M_1	0.594	C_{L_w}	7.9041 rad ⁻¹	C_{L_b}	5.3706 rad ⁻¹	$Z_{ref,off}$	0.2049	X_{ref_b}	3.6121	$dL/d\alpha$	0.3931	SM	56.96 %
$\bar{\alpha}$	155.41	C_{L_w}	7.9041 rad ⁻¹	C_{L_b}	5.3724 rad ⁻¹	$\bar{\alpha}_b$	7.7681 rad ⁻¹	C_{L_w}	5.7070 rad ⁻¹	\bar{V}_w	0.8040	$C_{L_{ref,off}}$	6.1586 rad ⁻¹
\bar{X}_{ref}	0.0702	C_{L_w}	7.9041 rad ⁻¹	X_{ref_w}	26.20 ft	C_{L_b}	7.7681 rad ⁻¹	C_{L_w}	0.7962 rad ⁻¹	X_w	30.22 ft	C_b	6.1586 rad ⁻¹
\bar{Z}_w	10.44 ft	C_{L_w}	5.3706 rad ⁻¹	Z_{ref_w}	0.2500	C_{L_b}	7.7681 rad ⁻¹	Z_{ref_b}	6.00 ft	$Z_{ref,off}$	0.6399	$C_{L_{ref,off}}$	3.5082 rad ⁻¹
X_{ref_w}	0.59 ft	$C_{L_w,off}$	5.3724 rad ⁻¹	$X_{ref,off}$	25.73 ft	X_{ref_b}	61.30 ft	$(dL/d\alpha)_{ref,off}$	0.3931	\bar{z}_w	0.6399	C_b	-3.5082 rad ⁻¹
High Lift Devices Table													
#	High Lift Device	$\bar{\alpha}_1$ %	$\bar{\alpha}_0$ %	$d\bar{\alpha}_w$ %	$\bar{\alpha}$ deg								
1	Single Slotted Flap	9.0	55.5	30.0	0.0								

Fig. 46 Angle of attack related derivatives

Angle of Attack Related Derivatives: Pitching Moment due to Thrust: Flight Condition 1										
Input Parameters										
Altitude	30000	ft	U_∞	350.00	fts	C_{L_1}	0.1076	Z_{cg}	2.95	ft
ΔT	0.0	deg F	$W_{current}$	37689.0	lb	X_{cg}	24.32	S_u	837.00	ft ²
Output Parameters										
\bar{C}_L	10.44	ft	\bar{q}_1	155.41	lb	D_{prop}	2492	hp	$(dC_L/dC_L)_{T_1}$	-0.0041
M_1	0.594		ZSH_{prop}	3109	hp	$(dC_L/dC_L)_{V_{prop}}$	0.0000		$(dC_L/dC_L)_V$	0.0000
									$C_{L_{prop}}$	-0.0251 rad ⁻¹
Propeller Table										
#	prop ft	prop ft	D prop ft	i prop deg	ψ prop deg	N_{n_prop}	rad ⁻¹	f_{inflow}	$df/d\alpha$	SHP set hp
Type	Input	Input	Input	Input	Input	Input	Input	Input	Input	%prop
1 Propeller: On	22.00	4.00	9.25	7.0	0.0	0.0000	1.0402	0.0000	1555	0.850
2 Propeller: On	22.00	4.00	9.25	7.0	0.0	0.0000	1.0402	0.0000	0	0.850
										5.7
										1246
										0

CU Boulder Advanced Aircraft Analysis 4.0 Project 12/12/18 10:11 am

Fig. 47 Angle of attack related derivatives

Rate of Angle of Attack Related Derivatives: Drag: Flight Condition 1										
Output Parameter										
$C_{D_{\alpha}}$	0.0000 rad ⁻¹									

Fig. 48 Angle of attack rate related derivatives

Rate of Angle of Attack Related Derivatives: Lift: Flight Condition 1														
Input Parameters														
Altitude	30000	ft	t_{ref_w}	0.93	X_{ref_w}	23.00	ft	S_0	190.00	ft ²				
ΔT	0.0	deg F	S_w	837.00	π^2	V_{ref_w}	0.00	ft	$(\text{IC})_v$	12.0	%			
U_1	350.00	fts	AR_w	8.00	$(\text{IC})_u$	12.00	%	I_0	1.00	$(\text{IC})_h$	12.0	%		
$C_{n_w}(\text{M}=0)$	6.3598	rad ⁻¹	λ_w	0.60	$(\text{IC})_p$	12.00	%	λ_{n_w}	0.0	deg	Z_{n_w}	6.00	ft	
$C_{n_w}(\text{M}>0)$	6.3598	rad ⁻¹	λ_{n_w}	0.0	deg	Z_{n_w}	2.00	ft	X_{ref_h}	60.00	ft	Γ_h	0.0	deg
									w_h	2.00	ft			
Output Parameters														
M_1	0.594		\tilde{Z}_w	10.44	ft	$C_{n_w}(\text{M}>0)C_{\text{cont}}$	4.5851	rad ⁻¹	C_{n_w}	7.7681	rad ⁻¹	\tilde{X}_{n_w}	3.6121	
X_{n_w}	26.20	ft	C_{n_w}	7.9041	rad ⁻¹	$C_{n_w(\text{con})}$	5.3706	rad ⁻¹	\tilde{C}_{n_w}	7.7681	rad ⁻¹	Z_{n_w}	6.00	ft
\tilde{Z}_{n_w}	0.2500		C_{n_w}	7.9041	rad ⁻¹	$C_{n_w(\text{M}>0)}$	4.5851	rad ⁻¹	\tilde{C}_{n_w}	7.7681	rad ⁻¹	C_{n_w}	5.7070	rad ⁻¹
\tilde{X}_{n_w}	0.0702		C_{n_w}	7.9041	rad ⁻¹	C_{n_w}	5.3706	rad ⁻¹	X_{ref_h}	61.30	ft	$(\text{d}u/\text{d}z)_\text{ref}$	0.3931	
									C_n	3.6077	rad ⁻¹			
High Lift Devices Table														
#	High Lift Device	η_1 %	η_0 %	q/c_w %	β deg									
1	Single Slotted Flap	9.0	55.5	30.0	0.0									

Fig. 49 Angle of attack rate related derivatives

Rate of Angle of Attack Related Derivatives: Pitching Moment: Flight Condition 1														
Input Parameters														
Altitude	30000	ft	t_{ref_w}	0.93	X_{ref_w}	23.00	ft	S_0	190.00	ft ²				
ΔT	0.0	deg F	S_w	837.00	π^2	V_{ref_w}	0.00	ft	$(\text{IC})_v$	12.0	%			
U_1	350.00	fts	AR_w	8.00	$(\text{IC})_u$	12.00	%	I_0	1.00	$(\text{IC})_h$	12.0	%		
$C_{n_w}(\text{M}=0)$	6.3598	rad ⁻¹	λ_w	0.60	$(\text{IC})_p$	12.00	%	λ_{n_w}	0.0	deg	Z_{n_w}	6.00	ft	
$C_{n_w}(\text{M}>0)$	6.3598	rad ⁻¹	λ_{n_w}	0.0	deg	Z_{n_w}	2.00	ft	X_{ref_h}	60.00	ft	Γ_h	0.0	deg
									w_h	2.00	ft			
Output Parameters														
M_1	0.594		\tilde{Z}_w	10.44	ft	$C_{n_w}(\text{M}>0)C_{\text{cont}}$	4.5851	rad ⁻¹	C_{n_w}	7.7681	rad ⁻¹	\tilde{X}_{n_w}	3.6121	
X_{n_w}	26.20	ft	C_{n_w}	7.9041	rad ⁻¹	$C_{n_w(\text{con})}$	5.3706	rad ⁻¹	\tilde{C}_{n_w}	7.7681	rad ⁻¹	Z_{n_w}	6.00	ft
\tilde{Z}_{n_w}	0.2500		C_{n_w}	7.9041	rad ⁻¹	$C_{n_w(\text{M}>0)}$	4.5851	rad ⁻¹	\tilde{C}_{n_w}	7.7681	rad ⁻¹	C_{n_w}	5.7070	rad ⁻¹
\tilde{X}_{n_w}	0.0702		C_{n_w}	7.9041	rad ⁻¹	C_{n_w}	5.3706	rad ⁻¹	X_{ref_h}	61.30	ft	$(\text{d}u/\text{d}z)_\text{ref}$	0.3931	
									C_n	-12.7779	rad ⁻¹			
High Lift Devices Table														
#	High Lift Device	η_1 %	η_0 %	q/c_w %	β deg									
1	Single Slotted Flap	9.0	55.5	30.0	0.0									

Fig. 50 Angle of attack rate related derivatives

Pitch Rate Related Derivatives: Drag: Flight Condition 1

Output Parameter

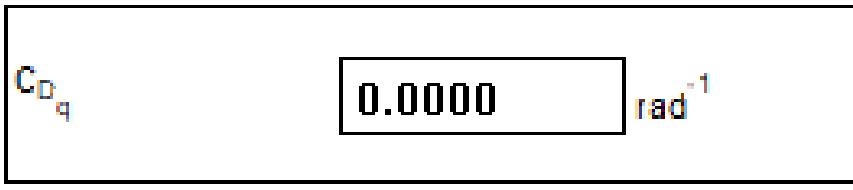


Fig. 51 Pitch rate related derivatives

Pitch Rate Related Derivatives: Lift Flight Condition 1											
Input Parameters											
Altitude	30000 ft	$C_{L_{\alpha_{\text{L}}}} @ M=0$	6.3598 rad ⁻¹	$\Delta_{\alpha_{\text{L}}}$	0.0 deg	S_b	190.00 m ²	$V_{\text{dih}_{\text{L}}}$	0.00 ft	η_b	1.000
ΔT	0.0 deg F	$t_{\text{sp}_{\text{L}}}$	0.93	$X_{\text{com}_{\text{L}}}$	23.00 ft	ΔR_b	7.00	$(V_C)_b$	12.0 %	$C_{L_{\alpha_{\text{L}}}} @ M=0$	6.2504 rad ⁻¹
U_1	350.00 kts	S_w	83.70 m ²	$V_{\text{dih}_{\text{L}}}$	0.00 ft	I_b	1.00	$(V_C)_b$	12.0 %	$C_{L_{\alpha_{\text{L}}}} @ M=0$	6.2504 rad ⁻¹
X_{cg}	24.32 ft	AR_w	8.00	$(V_C)_w$	12.00 %	$\Delta_{\alpha_{\text{L}}}$	0.0 deg	$Z_{\text{c}_{\text{L}}}$	6.00 ft	$t_{\text{sp}_{\text{L}}}$	1.00
$C_{L_{\alpha_{\text{L}}}} @ M=0$	6.3598 rad ⁻¹	I_w	0.60	$(V_C)_w$	12.00 %	X_{com_w}	60.00 ft	Γ_b	0.0 deg	w_b	2.00 ft
Output Parameters											
M_1	0.594	$C_{L_{\alpha_{\text{L}}}} @ M=0$	6.3598 rad ⁻¹	$C_{L_{\alpha_{\text{L}} w}}$	5.2621 rad ⁻¹	\bar{X}_{ω_w}	0.2500	X_{ω_L}	3.6121	$C_{L_{\alpha_{\text{L}}}}$	9.1763 rad ⁻¹
X_{cg}	0.0702	$C_{L_{\alpha_{\text{L}}}}$	7.9041 rad ⁻¹	$k_L - k_1$	0.913	$\delta_{\alpha_{\text{L}}}$	7.7681 rad ⁻¹	$C_{L_{\alpha_{\text{L}}}}$	5.7070 rad ⁻¹	$G_{L_{\alpha_{\text{L}}}}$	4.6958 rad ⁻¹
\bar{Z}_v	10.44 ft	S_{cap}	751.13 m ²	C_{ω_L}	0.0447 rad ⁻¹	C_{ω_L}	7.7681 rad ⁻¹	\bar{V}_b	0.8040	C_{ω_L}	0.2628 rad ⁻¹
$C_{L_{\alpha_{\text{L}}}}$	7.9041 rad ⁻¹	$C_{L_{\alpha_{\text{L}}}}$	10.20 ft	$K_{\text{ext}} + K_{\text{int}}$	1.18	δ_{ω_L}	7.7681 rad ⁻¹	$\bar{\Gamma}_b$	5.21 ft	$C_{L_{\alpha_{\text{L}}}}$	4.9586 rad ⁻¹
$C_{L_{\alpha_{\text{L}}}}$	7.9041 rad ⁻¹	$C_{L_{\alpha_{\text{L}}}}$	4.5851 rad ⁻¹	X_{ω_w}	26.20 ft	X_{ω_L}	61.30 ft	$C_{L_{\alpha_{\text{L}}}}$	81.0235 rad ⁻¹	C_{ω_L}	14.1354 rad ⁻¹
High Lift Devices Table											
#	High Lift Device	η_1 %	η_0 %	η_{L} %	η_{L} deg						
1	Single Slotted Flap	9.0	55.5	30.0	0.0						

Fig. 52 Pitch rate related derivatives

Pitch Rate Related Derivatives: Pitching Moment: Flight Condition 1											
Input Parameters											
Altitude	30000 ft	$t_{\text{sp}_{\text{M}}}$	0.91	$X_{\text{com}_{\text{M}}}$	23.00 ft	S_b	190.00 m ²	$(V_C)_b$	12.0 %	$C_{L_{\alpha_{\text{M}}}} @ M=0$	6.2504 rad ⁻¹
ΔT	0.0 deg F	$t_{\text{sp}_{\text{M}}}$	0.93	$V_{\text{dih}_{\text{M}}}$	0.00 ft	ΔR_b	7.00	$(V_C)_b$	12.0 %	$t_{\text{sp}_{\text{M}}}$	1.00
U_1	350.00 kts	S_w	83.70 m ²	$(V_C)_w$	12.00 %	I_b	1.00	$Z_{\text{c}_{\text{M}}}$	6.00 ft	w_b	2.00 ft
X_{cg}	24.32 ft	AR_w	8.00	$(V_C)_w$	12.00 %	$\Delta_{\alpha_{\text{M}}}$	0.0 deg	Γ_b	0.0 deg	X_{com_w}	0.00 ft
$C_{L_{\alpha_{\text{M}}}} @ M=0$	6.3598 rad ⁻¹	I_w	0.60	w_b	6.83 ft	X_{ω_w}	60.00 ft	η_b	1.000	\dot{S}_T	55.00 ft
$C_{L_{\alpha_{\text{M}}}} @ M=0$	6.3598 rad ⁻¹	$\Delta_{\alpha_{\text{M}}}$	0.0 deg	$C_{L_{\alpha_{\text{M}}}}$	5.3724 rad ⁻¹	$V_{\text{dih}_{\text{M}}}$	0.00 ft	$C_{L_{\alpha_{\text{M}}}} @ M=0$	6.2504 rad ⁻¹	ΔX_{ω_L}	-0.0451
Output Parameters											
M_1	0.594	$C_{L_{\alpha_{\text{M}}}}$	7.9041 rad ⁻¹	$\bar{Z}_{\text{c}_{\text{M}}}$	10.20 ft	\bar{X}_{ω_w}	0.2500	X_{ω_M}	61.30 ft	\bar{Z}_v	5.21 ft
X_{cg}	0.0702	$C_{L_{\alpha_{\text{M}}}} @ M=0$	6.3598 rad ⁻¹	C_{ω_M}	0.2422 rad ⁻¹	C_{ω_M}	7.7681 rad ⁻¹	X_{ω_M}	3.6121	C_{ω_M}	-143.1850 rad ⁻¹
\bar{Z}_v	10.44 ft	$C_{L_{\alpha_{\text{M}}}}$	7.9041 rad ⁻¹	$K_{\text{ext}} + K_{\text{int}}$	1.18	δ_{ω_M}	7.7681 rad ⁻¹	C_{ω_M}	5.7070 rad ⁻¹	C_{ω_M}	-32.5032 rad ⁻¹
$C_{L_{\alpha_{\text{M}}}}$	7.9041 rad ⁻¹	S_{cap}	751.13 m ²	X_{ω_w}	26.20 ft	$\delta_{\alpha_{\text{M}}}$	7.7681 rad ⁻¹	\bar{V}_b	0.8040	C_{ω_M}	-1.3600 rad ⁻¹

Fig. 53 Pitch rate related derivatives

Fuselage Geometry: Flight Condition 1														
Input Parameters														
X_{fus_1}	0.00	ft	Z_{fus_1}	2.00	ft	X_{fus_2}	23.00	ft	X_{fus_3}	60.00	ft	X_{fus_4}	60.00	ft
Y_{fus_1}	0.00	ft		0.00	deg	Z_{fus_1}	12.79	ft	Z_{fus_2}	5.21	ft	Z_{fus_3}	7.51	ft
												$(X, Z)_{\text{fus}}$		
												b_{fus}	8	
Output Parameters														
b_1	55.00	ft	S_{max}		ft ²	X_1		ft	X_{fus}		ft	b_{fus}	2.50	ft
b_{fus}	2.00	ft	S_{fus}	383.07	ft ²	X_2	49.72	ft	b_{fus}	6.70	ft	D_{fus}	6.83	ft
w_{fus}	6.78	ft	S_{fus}		ft ²	S_0	20.49	ft ²	b_{fus}	5.00	ft	Z_{fus}	5.00	ft
S_{fus}		ft ²	S_{fus}		ft ²	V_1		ft ³	Z_{fus}	2.50	ft	b_{fus}		Coordinates Undefined

Fuselage Table: double click for Cross-Section Dialog

Fuselage	x_{fus_1} ft	y_{fus_1} ft	z_{fus_1} ft	y_{fus_2} ft	z_{fus_2} ft	y_{fus_3} ft	z_{fus_3} ft	y_{fus_4} ft	z_{fus_4} ft	y_{fus_5} ft	z_{fus_5} ft	A_{fus} ft ²	s_{fus} ft
Section	Input	Output	Output										
1	0.0000										0.00		
2	4.5000										19.60		
3	15.0000										36.30		
4	47.0000										36.30		
5	55.0000										9.18		
6	68.0000										3.14		
7	66.0000										3.14		
8	66.1000										0.00		

Fig. 54 Fuselage geometry

Sideslip Related Derivatives: Sideforce: Flight Condition 1														
Input Parameters														
Altitude	30000	ft	Δ_{roll}	0.0	deg	Γ_{ad}	5.0	deg	S_c	137.00	ft ²	$C_{D_{\text{fus}}(M=0)}$	6.2800	rad ⁻¹
ΔT	0.0	deg F	Z_{fus}	2.50	ft	S_0	190.00	ft ²	AR_{fus}	3.00		r_{fus}	1.00	
U_1	350.00	fts	Z_{fus}	2.00	ft	X_{fus}	61.30	ft	b_{fus}	0.80		$(IC)_{\text{fus}}$	12.0	%
S_w	837.00	ft ²	w_{fus}	6.83	ft	Z_{fus}	6.00	ft	Δ_{roll}	5.0	deg	$(IC)_{\text{fus}}$	12.0	%
AR_{fus}	8.00		Γ_{ad}	5.0	deg	Z_{fus}	5.00	ft	$C_{D_{\text{fus}}(M=0)}$	6.2800	rad ⁻¹	η_{fus}	1.000	
												b_{fus}	2.50	
Output Parameters														
Z_u	0.00	ft	$C_{D_{\text{fus}}}$	7.8049	rad ⁻¹	$C_{D_{\text{fus}}}$	-4.5029	rad ⁻¹	$k_2 - k_1$	0.913		$C_{D_{\text{fus}}}$	-0.0590	rad ⁻¹
M_1	0.594		$C_{D_{\text{fus}}}$	7.8049	rad ⁻¹	x/C_c	0.2760		$C_{D_{\text{fus}}}$	0.0447	rad ⁻¹	$C_{D_{\text{fus}}}$	-0.8302	rad ⁻¹
AR_{fus}	4.32		$C_{D_{\text{fus}}}$	7.8049	rad ⁻¹	$(goldS)_c$	-0.1264		$C_{D_{\text{fus}}}$	0.0287	rad ⁻¹	$C_{D_{\text{fus}}}$	-0.9179	rad ⁻¹

Fig. 55 Sideslip related derivatives

Sideslip Related Derivatives: Rolling Moment: Flight Condition 1														
Input Parameters														
Altitude	30000	ft	Δ_{roll}	0.50		$C_{D_{\text{fus}}(M=0)}$	6.3598	rad ⁻¹	Δ_{roll}	0.0	deg	X_{fus}	60.00	ft
ΔT	0.0	deg F	Δ_{roll}	0.0	deg	$C_{D_{\text{fus}}(M=0)}$	6.3598	rad ⁻¹	Γ_{ad}	0.0	deg	$C_{D_{\text{fus}}(M=0)}$	6.2800	rad ⁻¹
U_1	350.00	fts	Γ_{ad}	5.0	deg	X_{fus}	0.00	ft	Z_{fus}	0.0	deg	S_c	137.00	ft ²
α	0.00	deg	Γ_{ad}	5.0	deg	Z_{fus}	2.50	ft	Z_{fus}	6.00	ft	AR_{fus}	3.00	
$C_{L_{\text{roll}}, \text{roll}, \text{ref}}$	0.1075		Δ_{roll}	0.0	deg	$C_{D_{\text{fus}}}$	-0.0798		Z_{fus}	5.00	ft	$(IC)_{\text{fus}}$	0.80	
$\Delta C_{L_{\text{roll}}}$	0.0000		Z_{fus}	2.00	ft	S_0	190.00	ft ²	X_{fus}	61.30	ft	Δ_{roll}	5.0	deg
S_w	837.00	ft ²	X_{fus}	23.00	ft	AR_{fus}	7.00		Z_{fus}	6.00	ft	X_{fus}	60.00	ft
AR_{fus}	8.00		η_{fus}	0.0	%	Z_u	1.00		Z_{fus}	5.00	ft	Z_{fus}	15.00	ft
Output Parameters														
M_1	0.594		$C_{D_{\text{fus}}}$	7.9041	rad ⁻¹	AR_{fus}	4.32		$C_{D_{\text{fus}}}$	7.8049	rad ⁻¹	$C_{D_{\text{fus}}}$	-4.5029	rad ⁻¹
$C_{D_{\text{fus}}}$	7.9041	rad ⁻¹	X_{fus}	62.73	ft	X/C_c	0.2760		$C_{D_{\text{fus}}}$	7.8049	rad ⁻¹	$C_{D_{\text{fus}}}$	-0.8302	rad ⁻¹
$C_{D_{\text{fus}}}$	7.9041	rad ⁻¹	Z_{fus}	24.76	ft	$(goldS)_c$	-0.1264		$C_{D_{\text{fus}}}$	7.8049	rad ⁻¹	$C_{D_{\text{fus}}}$	-0.0790	rad ⁻¹

Fig. 56 Sideslip related derivatives

Sideslip Related Derivatives: Yawing Moment: Flight Condition 1													
Input Parameters													
Altitude	30000	ft	$\dot{\alpha}_w$	0.60	Z_{α_w}	6.00	X_{α_w}	60.00	%	$(DC)_w$	12.0		
ΔT	0.0	deg F	$\Delta \alpha_{L_d}$	0.0	deg	Z_{L_d}	5.00	n	η_w	1.000	R_{T_d}	383.07	
U_1	350.00	fts	$Z_{C_{L_d}}$	2.00	n	S_v	137.00	ft^2	$C_{L_d, \text{M=0}}$	6.2800	rad^{-1}	k	55.00
α	0.00	deg	$Z_{C_{D_s}}$	2.50	n	AR_w	3.00		$C_{D_s, \text{M=0}}$	6.2800	rad^{-1}	h_w	2.50
S_w	937.00	ft^2	S_h	190.00	ft^2	L_w	0.80		t_{α_w}	1.00		h_{ext}	2.00
AR_w	8.00		X_{α_w}	61.30	n	$\Delta \alpha_{L_d}$	5.0	deg	$(DC)_{L_d}$	12.0	%	X_{D_d}	24.32
												w_{ext}	6.78
Output Parameters													
M_1	0.594		$Z_{C_{D_s}}$	24.76	n	C_{D_s}	7.8049	rad^{-1}	W_{C_s}	0.2760		$K_{C_{D_s}}$	-0.00029
Re	93.1248 $\times 10^6$		AR_{ref}	4.32		C_{L_d}	7.8049	rad^{-1}	$(DC)_{L_d}$	0.1264		C_{β}	1.92878
$X_{C_{D_s}}$	62.73	n	$C_{N_{\alpha}}$	7.8049	rad^{-1}	C_{β}	-4.5029	rad^{-1}	C_{β_w}	-0.8302	rad^{-1}	C_{β_h}	0.0098

Fig. 57 Sideslip related derivatives

Sideslip Related Derivatives: Sideforce due to Thrust: Flight Condition 1											
Input Parameter											
S_w	837.00 ft^2										
Output Parameter											
$C_{Y_T \beta}$	0.0000 rad^{-1}										
Propeller Table											
#	Type	D_{prop}	ft	f_{Inflow}	$C_{N_{\alpha}} \text{ prop}$	rad^{-1}					
1	Propeller: On	9.25		1.0402	0.0000						
2	Propeller: On	9.25		1.0402	0.0000						

Fig. 58 Sideslip related derivatives

Sideslip Related Derivatives: Yawing Moment due to Thrust: Flight Condition 1								
Input Parameters								
X _{cg}	24.32 ft	Y _{cg}	-0.11 ft	S _w	837.00 ft ²	AR _w	8.00	
Output Parameter								
C _{L_{T_p}}	0.0000 rad ⁻¹							
Propeller Table								
#	Type	X _{prop} ft	Y _{prop} ft	i _{prop} deg	ψ _{prop} deg	D _{prop} ft	f _{Inflow}	C _{N_{prop}} rad ⁻¹
1	Propeller: On	22.00	9.01	7.0	0.0	9.25	1.0402	0.0000
2	Propeller: On	22.00	-9.01	7.0	0.0	9.25	1.0402	0.0000

Fig. 59 Sideslip related derivatives

Subsonic Horizontal Tail Drag Coefficient Prediction: Flight Condition 1							
Input Parameters							
Altitude	30000 ft	S _w	837.00 ft ²	A _{ref_b}	0.0 deg	\bar{c}_n	5.21 ft
ΔT	0.0 deg F	S _t	190.00 ft ²	A _{ref_t}	0.0 deg	(R _{ref}) _t	1.000 %
U ₁	350.00 kts	AR _t	7.00	(R _{ref}) _b	12.00 %	S _{ref_t}	369.94 ft ²
C _{D_b}	-0.0798	β_t	1.00	k _{rand}	0.01333 10 ⁻³ ft	\bar{c}_{Db}	5.21 ft
						C _{D_b}	5.7070 rad ⁻¹
Output Parameters							
M ₁	0.594	C _{D_b}	0.0028	ρ_t	0.9956	\bar{C}_{Dbh}	0.0017
						C _{D_bh}	0.0001

Fig. 60 Horizontal stabilizer drag coefficient

Rate of Sideslip Related Derivatives: Sideforce: Flight Condition 1							
Input Parameters							
Altitude	30000 ft	AR _w	8.00	Z _{z_w}	2.00 ft	V _w	61.30 ft
ΔT	0.0 deg F	β_w	0.60	Z _{z_w}	2.50 ft	Z _{z_b}	6.00 ft
U ₁	350.00 kts	A _{ref_w}	0.0 deg	Z _{z_w}	26.20 ft	Z _{z_b}	5.00 ft
α	0.00 deg	Γ_w	5.0 deg	Z _{z_w}	3.64 ft	S _w	137.00 ft ²
S _w	837.00 ft ²	α_{zw	0.0 deg	S _w	190.00 ft ²	AR _t	3.00
						C _{D_w} (M=0)	6.2800 rad ⁻¹
Output Parameters							
M ₁	0.594	Z _{z_w}	24.76 ft	C _{D_w}	7.0049 rad ⁻¹	C _{D_b}	7.0049 rad ⁻¹
X _w	62.73 ft	AR _{wf}	4.32	C _{D_w}	7.0049 rad ⁻¹	C _{D_b}	-4.5029 rad ⁻¹
						C _{D_{wf}}	-0.2389 rad ⁻¹
						α_{zw	0.0109
						C _{D_{wf}}	-0.0066 rad ⁻¹

Fig. 61 Sideslip rate related derivatives

Rate of Sideslip Related Derivatives: Rolling Moment: Flight Condition 1											
Input Parameters											
Altitude	30000	ft	AR _w	8.00	Z _{e₁} _{1g}	2.00	ft	X _{m₁}	61.30	ft	
ΔT	0.0	deg F	I _w	0.50	Z _{e₁} _w	2.50	ft	Z _{e₁} _{1g}	6.00	ft	
U ₁	350.00	fts	A _{roll_w}	0.0	deg	X _{m₁}	26.20	ft	Z _{e₁} _w	5.00	ft
α	0.00	deg	I _z	5.0	deg	Z _{e₁} _w	3.64	ft	S _z	137.00	ft ²
S _w	937.00	ft ²	C _{g_w}	0.0	deg	S _z	190.00	ft ³	AR _w	3.00	
								C _{g_w} (M=0)	6.2800	rad ⁻¹	
								D _{roll_w}	6.83	ft	

Output Parameters											
M ₁	0.594		AR _{ref}	4.32	C _{g_w}	7.8049	rad ⁻¹	D _{roll_w}	-0.2389	deg ⁻¹	
X _{m₁}	62.73	ft	C _{g_w}	7.8049	rad ⁻¹	C _{l₃}	-4.5029	rad ⁻¹	D _{roll_w}	0.0012	deg ⁻¹
Z _{e₁} _w	24.76	ft	C _{g_w}	7.8049	rad ⁻¹	D _{roll_w}	-0.0012	deg ⁻¹	D _{roll_w}	0.0109	
									C ₃	-0.0017	rad ⁻¹

Fig. 62 Sideslip rate related derivatives

Rate of Sideslip Related Derivatives: Yawing Moment: Flight Condition 1											
Input Parameters											
Altitude	30000	ft	AR _w	8.00	Z _{e₁} _{1g}	2.00	ft	X _{m₁}	61.30	ft	
ΔT	0.0	deg F	I _w	0.50	Z _{e₁} _w	2.50	ft	Z _{e₁} _{1g}	6.00	ft	
U ₁	350.00	fts	A _{roll_w}	0.0	deg	X _{m₁}	26.20	ft	Z _{e₁} _w	5.00	ft
α	0.00	deg	I _z	5.0	deg	Z _{e₁} _w	3.64	ft	S _z	137.00	ft ²
S _w	937.00	ft ²	C _{g_w}	0.0	deg	S _z	190.00	ft ³	AR _w	3.00	
								C _{g_w} (M=0)	6.2800	rad ⁻¹	
								D _{roll_w}	6.83	ft	

Output Parameters											
M ₁	0.594		AR _{ref}	4.32	C _{g_w}	7.8049	rad ⁻¹	D _{roll_w}	-0.2389	deg ⁻¹	
X _{m₁}	62.73	ft	C _{g_w}	7.8049	rad ⁻¹	C _{l₃}	-4.5029	rad ⁻¹	D _{roll_w}	0.0012	deg ⁻¹
Z _{e₁} _w	24.76	ft	C _{g_w}	7.8049	rad ⁻¹	D _{roll_w}	-0.0012	deg ⁻¹	D _{roll_w}	0.0109	
									C ₃	-0.0029	rad ⁻¹

Fig. 63 Sideslip rate related derivatives

Sideslip Related Derivatives: Sideforce due to Thrust: Flight Condition 1

Input Parameter

S_w	837.00	ft^2
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Output Parameter

$C_{Y_T \beta}$	0.0000	rad^{-1}
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Propeller Table

#	Type	D_{prop} ft	f_{Inflow}	$C_{N_a} \text{ prop}$ rad^{-1}
1	Propeller: On	9.25	1.0402	0.0000
2	Propeller: On	9.25	1.0402	0.0000

Fig. 64 Sideslip related derivatives

Sideslip Related Derivatives: Yawing Moment due to Thrust: Flight Condition 1					
Input Parameters					
X_{cg}	24.32	ft	Y_{cg}	-0.11	ft
S_w	837.00	ft^2	AR_w	8.00	
Output Parameter					
$C_{n_T \beta}$	0.0000	rad^{-1}			
Propeller Table					
#	Type	X_{prop} ft	Y_{prop} ft	i_{prop} deg	ψ_{prop} deg
1	Propeller: On	22.00	9.01	7.0	0.0
2	Propeller: On	22.00	-9.01	7.0	0.0
				D_{prop} ft	f_{Inflow}
				9.25	1.0402
					$C_{N_a} \text{ prop}$ rad^{-1}
					0.0000

Fig. 65 Sideslip related derivatives

Roll Rate Related Derivatives: Sideforce: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	α	0.00 deg	$Z_{e_{\alpha}}$	2.50 ft	$t_{e_{\alpha e_{\alpha}}}$	0.91	S_b	137.00 ft ²
ΔT	0.0 deg F	S_w	837.00 ft ²	$Z_{e_{\alpha}}$	0.60	S_b	190.00 ft ²	$A R_b$	3.00
U_1	350.00 kts	$A R_w$	8.00	$T_{e_{\alpha}}$	5.0 deg	$X_{e_{\alpha}}$	61.30 ft	$C_{e_{\alpha} \text{GM=0}}$	6.2800 rad ⁻¹
X_{C_d}	24.32 ft	$\lambda_{e_{\alpha}}$	0.0 deg	$C_{e_{\alpha} \text{GM=0}}$	6.3598 rad ⁻¹	$Z_{e_{\alpha}}$	6.00 ft	$\lambda_{e_{\alpha}}$	5.0 deg
$Z_{e_{\alpha}}$	2.95 ft	$Z_{e_{\alpha} e_{\alpha}}$	2.00 ft	$C_{e_{\alpha} \text{GM=0}}$	6.3598 rad ⁻¹	$Z_{e_{\alpha}}$	5.00 ft	$X_{e_{\alpha} e_{\alpha}}$	60.00 ft
								$(U C)_{e_{\alpha}}$	12.0 %
Output Parameters									
M_1	0.594	$C_{e_{\alpha}}$	7.9041 rad ⁻¹	$A R_{e_{\alpha}}$	4.32	$C_{e_{\alpha}}$	7.8049 rad ⁻¹	$(g \delta \beta)_{e_{\alpha}}$	0.1264
$C_{e_{\alpha} e_{\alpha}}$	7.9041 rad ⁻¹	$X_{e_{\alpha}}$	62.73 ft	$Z_{e_{\alpha}}$	7.8049 rad ⁻¹	$C_{e_{\alpha}}$	-4.5029 rad ⁻¹	$C_{e_{\alpha}}$	-0.8302 rad ⁻¹
$C_{e_{\alpha} e_{\alpha}}$	7.9041 rad ⁻¹	$Z_{e_{\alpha}}$	24.76 ft	$C_{e_{\alpha}}$	7.8049 rad ⁻¹	$X_{e_{\alpha}}$	0.2760	$C_{e_{\alpha}}$	-0.1342 rad ⁻¹

Fig. 66 Roll rate related derivatives

Roll Rate Related Derivatives: Rolling Moment: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	$A R_w$	8.00	$C_{e_{\alpha} \text{GM=0}}$	6.3598 rad ⁻¹	$I_{e_{\alpha}}$	1.00	$t_{e_{\alpha} e_{\alpha}}$	1.00
ΔT	0.0 deg F	$I_{e_{\alpha}}$	0.60	$t_{e_{\alpha} e_{\alpha}}$	0.91	$\lambda_{e_{\alpha}}$	0.0 deg	$t_{e_{\alpha} e_{\alpha}}$	1.00
U_1	350.00 kts	$\lambda_{e_{\alpha}}$	0.0 deg	$t_{e_{\alpha} e_{\alpha}}$	0.93	$T_{e_{\alpha}}$	0.0 deg	$X_{e_{\alpha}}$	5.7070 rad ⁻¹
α	0.00 deg	$T_{e_{\alpha}}$	5.0 deg	$C_{e_{\alpha}}$	5.3706 rad ⁻¹	$Z_{e_{\alpha}}$	6.00 ft	$X_{e_{\alpha}}$	61.30 ft
$C_{e_{\alpha} e_{\alpha}}$	-3.0 deg	$Z_{e_{\alpha}}$	2.00 ft	$Z_{e_{\alpha}}$	0.0037	w_L	2.00 ft	$Z_{e_{\alpha}}$	6.00 ft
$I_{e_{\alpha}}$	-1.0 deg	$(U C)_{e_{\alpha}}$	12.00 %	$Z_{e_{\alpha}}$	0.0000	$(U C)_{e_{\alpha}}$	12.00 %	$Z_{e_{\alpha}}$	0.0017
$C_{e_{\alpha} e_{\alpha}}$	5.3706 rad ⁻¹	$(U C)_{e_{\alpha}}$	12.00 %	$C_{e_{\alpha}}$	-0.0798	$(U C)_{e_{\alpha}}$	12.00 %	S_b	137.00 ft ²
ΔC_{Ld}	0.0000	$Z_{e_{\alpha}}$	2.50 ft	S_b	190.00 ft ²	$C_{e_{\alpha} \text{GM=0}}$	6.2504 rad ⁻¹	$A R_b$	3.00
S_b	837.00 ft ²	$C_{e_{\alpha} \text{GM=0}}$	6.3598 rad ⁻¹	$A R_b$	7.00	$C_{e_{\alpha} \text{GM=0}}$	6.2504 rad ⁻¹	$I_{e_{\alpha}}$	0.80
								$(g \delta \beta)_{e_{\alpha}}$	1.000
Output Parameters									
M_1	0.594	$C_{e_{\alpha}}$	6.3598 rad ⁻¹	$C_{e_{\alpha}}$	6.2504 rad ⁻¹	$A R_{e_{\alpha}}$	4.32	$C_{e_{\alpha}}$	7.8049 rad ⁻¹
$C_{e_{\alpha} \text{GM=0}}$	0.1875	$C_{e_{\alpha}}$	7.9041 rad ⁻¹	$C_{e_{\alpha}}$	7.7681 rad ⁻¹	$C_{e_{\alpha}}$	7.8049 rad ⁻¹	$C_{e_{\alpha}}$	-4.5029 rad ⁻¹
$C_{e_{\alpha}}$	7.9041 rad ⁻¹	$C_{e_{\alpha}}$	7.7681 rad ⁻¹	$X_{e_{\alpha}}$	62.73 ft	$C_{e_{\alpha}}$	7.8049 rad ⁻¹	$X_{e_{\alpha}}$	0.2760
$C_{e_{\alpha}}$	7.9041 rad ⁻¹	$C_{e_{\alpha}}$	7.7681 rad ⁻¹	$Z_{e_{\alpha}}$	24.76 ft	$C_{e_{\alpha} \text{GM=0}}$	6.2800 rad ⁻¹	$(g \delta \beta)_{e_{\alpha}}$	-0.1264
High Lift Devices Table									
#	High Lift Device	C_{Ld} %	$S_{w_{Hd}}$ $R_{w_{Hd}}$	b deg					
1	Single Slotted Flap	30.0	0.506	0.0					

Fig. 67 Roll rate related derivatives

Roll Rate Related Derivatives: Yawing Moment: Flight Condition 1											
Input Parameters											
Altitude	30000 ft	$C_{L_{\text{roll},\text{open}}}$	5.3706 rad ⁻¹	$Z_{e_{\text{roll}}}$	2.00 ft	$Z_{e_{\text{roll}}}$	6.00 ft	X_{open}	60.00 ft	$(\partial C_L)/(\partial \alpha)$	12.0 %
ΔT	0.0 deg F	S_w	837.00 ft ²	$Z_{e_{\text{roll}}}$	2.50 ft	$Z_{e_{\text{roll}}}$	5.00 ft	Z_{open}	15.00 ft	η_v	1.000
U_1	350.00 kts	AR_w	8.00	$C_{L_{\text{roll},\text{GM=0}}}$	6.3598 rad ⁻¹	S_v	137.00 ft ²	$C_{L_{\text{roll},\text{GM=0}}}$	6.2800 rad ⁻¹	h_w	2.50 ft
α	0.00 deg	λ_{roll}	0.60	$C_{L_{\text{roll},\text{GM=0}}}$	6.3598 rad ⁻¹	AR_v	3.00	$C_{L_{\text{roll},\text{GM=0}}}$	6.2800 rad ⁻¹	h_v	2.00 ft
$a_{\text{roll,open}}$	-3.0 deg	λ_{roll}	0.0 deg	S_v	190.00 ft ²	λ_v	0.80	t_{roll}	1.00	X_{roll}	24.32 ft
ι_w	-1.0 deg	λ_{roll}	0.0 deg	X_{roll}	61.30 ft	λ_{roll}	5.0 deg	$(\partial C_L)/(\partial \iota_w)$	12.0 %	Z_{roll}	2.95 ft
Output Parameters											
M_1	0.594	$C_{L_{\text{roll}}}$	7.9041 rad ⁻¹	$Z_{e_{\text{roll}}}$	24.76 ft	$C_{L_{\text{roll}}}$	7.8049 rad ⁻¹	X/C_v	0.2760	$C_{L_{\text{roll}}}$	0.0000 rad ⁻¹
$C_{w(\text{roll,full})}$	0.1875	$C_{L_{\text{roll}}}$	7.9041 rad ⁻¹	AR_{eff}	4.32	$C_{L_{\text{roll}}}$	7.8049 rad ⁻¹	$(\partial C/L)/(\partial S_v)$	-0.1264	$C_{L_{\text{roll}}}$	0.0193 rad ⁻¹
$C_{L_{\text{roll}}}$	7.9041 rad ⁻¹	X_{roll}	62.73 ft	$C_{L_{\text{roll}}}$	7.8049 rad ⁻¹	$C_{L_{\text{roll}}}$	-4.5029 rad ⁻¹	$C_{D_{\text{roll}}}$	-0.8302 rad ⁻¹	$C_{L_{\text{roll}}}$	0.0000 rad ⁻¹
High Lift Devices Table											
#	High Lift Device	η_1 %	η_0 %	cL/c_w %	β deg						
1	Single Slotted Flap	9.0	55.5	30.0	0.0						

Fig. 68 Roll rate related derivatives

Yaw Rate Related Derivatives: Sideforce: Flight Condition 1											
Input Parameters											
Altitude	30000 ft	α	0.00 deg	$Z_{e_{\text{roll}}}$	2.50 ft	S_v	137.00 ft ²	Z_{open}	15.00 ft	$(\partial C_L)/(\partial \alpha)$	12.0 %
ΔT	0.0 deg F	S_w	837.00 ft ²	S_v	190.00 ft ²	AR_v	3.00	$C_{L_{\text{roll},\text{GM=0}}}$	6.2800 rad ⁻¹	η_v	1.000
U_1	350.00 kts	AR_w	8.00	X_{roll}	61.30 ft	λ_v	0.80	$C_{L_{\text{roll},\text{GM=0}}}$	6.2800 rad ⁻¹	h_w	2.50 ft
X_{roll}	24.32 ft	λ_{roll}	0.0 deg	$Z_{e_{\text{roll}}}$	6.00 ft	λ_{roll}	5.0 deg	t_{roll}	1.00	h_v	2.00 ft
Z_{roll}	2.95 ft	$Z_{e_{\text{roll}}}$	2.00 ft	$Z_{e_{\text{roll}}}$	5.00 ft	X_{open}	60.00 ft	$(\partial C_L)/(\partial \iota_w)$	12.0 %		
Output Parameters											
M_1	0.594	$Z_{e_{\text{roll}}}$	24.76 ft	$C_{L_{\text{roll}}}$	7.8049 rad ⁻¹	$C_{L_{\text{roll}}}$	7.8049 rad ⁻¹	X/C_v	0.2760	$C_{L_{\text{roll}}}$	-0.8302 rad ⁻¹
X_{roll}	62.73 ft	AR_{eff}	4.32	$C_{L_{\text{roll}}}$	7.8049 rad ⁻¹	$C_{L_{\text{roll}}}$	-4.5029 rad ⁻¹	$(\partial C/L)/(\partial S_v)$	-0.1264	$C_{L_{\text{roll}}}$	0.7794 rad ⁻¹

Fig. 69 Yaw rate related derivatives

Yaw Rate Related Derivatives: Rolling Moment: Flight Condition 1											
Input Parameters											
Altitude	30000 ft	$C_{L_{\text{roll},\text{open}}}$	5.3706 rad ⁻¹	z_w	0.0 deg	X_{roll}	61.30 ft	λ_{roll}	5.0 deg	$(\partial C_L)/(\partial \alpha)$	12.0 %
ΔT	0.0 deg F	S_w	837.00 ft ²	$Z_{e_{\text{roll}}}$	2.00 ft	$Z_{e_{\text{roll}}}$	6.00 ft	X_{open}	60.00 ft	$(\partial C_L)/(\partial \alpha)$	12.0 %
U_1	350.00 kts	AR_w	8.00	$Z_{e_{\text{roll}}}$	2.50 ft	$Z_{e_{\text{roll}}}$	5.00 ft	Z_{open}	15.00 ft	η_v	1.000
α	0.00 deg	λ_{roll}	0.60	$C_{L_{\text{roll},\text{GM=0}}}$	6.3598 rad ⁻¹	S_v	137.00 ft ²	$C_{L_{\text{roll},\text{GM=0}}}$	6.2800 rad ⁻¹	h_w	2.50 ft
$a_{\text{roll,open}}$	-3.0 deg	λ_{roll}	0.0 deg	$C_{L_{\text{roll},\text{GM=0}}}$	6.3598 rad ⁻¹	AR_v	3.00	$C_{L_{\text{roll},\text{GM=0}}}$	6.2800 rad ⁻¹	h_v	2.00 ft
ι_w	-1.0 deg	λ_{roll}	5.0 deg	S_v	190.00 ft ²	λ_v	0.80	t_{roll}	1.00	X_{roll}	24.32 ft
Output Parameters											
M_1	0.594	$C_{L_{\text{roll}}}$	7.9041 rad ⁻¹	$Z_{e_{\text{roll}}}$	24.76 ft	$C_{L_{\text{roll}}}$	7.8049 rad ⁻¹	X/C_v	0.2760	$C_{L_{\text{roll}}}$	0.0000 rad ⁻¹
$C_{w(\text{roll,full})}$	0.1875	$C_{L_{\text{roll}}}$	7.9041 rad ⁻¹	AR_{eff}	4.32	$C_{L_{\text{roll}}}$	7.8049 rad ⁻¹	$(\partial C/L)/(\partial S_v)$	-0.1264	$C_{L_{\text{roll}}}$	0.0506 rad ⁻¹
$C_{L_{\text{roll}}}$	7.9041 rad ⁻¹	X_{roll}	62.73 ft	$C_{L_{\text{roll}}}$	7.8049 rad ⁻¹	$C_{L_{\text{roll}}}$	-4.5029 rad ⁻¹	$C_{D_{\text{roll}}}$	-0.8302 rad ⁻¹	$C_{L_{\text{roll}}}$	0.2077 rad ⁻¹
High Lift Devices Table											
#	High Lift Device	η_1 %	η_0 %	cL/c_w %	β deg						
1	Single Slotted Flap	9.0	55.5	30.0	0.0						

Fig. 70 Yaw rate related derivatives

Yaw Rate Related Derivatives: Yawing Moment: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	$\dot{\alpha}_e$	-1.0 deg	$\Delta C_{l_{\alpha_e}}$	0.0 rad ⁻¹	$X_{\alpha_{l_{\alpha_e}}}$	61.30 %	$\Delta C_{l_{\alpha_e}(\bar{M}=0)}$	6.2800 rad ⁻¹
ΔT	0.0 deg F	$C_{l_{\alpha_e} \text{ clean}}$	5.3706 rad ⁻¹	$Z_{l_{\alpha_e}}$	2.00 %	$Z_{\alpha_{l_{\alpha_e}}}$	6.00 %	$\Delta_{l_{\alpha_e}}$	5.0 deg
U_1	350.00 kts	S_a	837.00 ft ²	$Z_{l_{\alpha_e}}$	2.50 %	$Z_{l_{\alpha_e}}$	5.00 %	$X_{\alpha_{l_{\alpha_e}}}$	60.00 %
α	0.00 deg	AR _a	8.00	$\tilde{C}_{l_{\alpha_e}}$	0.0037	S_a	137.00 ft ²	$Z_{\alpha_{l_{\alpha_e}}}$	15.00 %
α_{clean}	-3.0 deg	$\dot{\alpha}_e$	0.50	S_a	190.00 %	AR _a	3.00	$\Delta C_{l_{\alpha_e}(\bar{M}=0)}$	6.2800 rad ⁻¹
Output Parameters									
M_1	0.594	$Z_{l_{\alpha_e}}$	24.76 %	$C_{l_{\alpha_e}}$	7.8049 rad ⁻¹	$X_{C_{l_{\alpha_e}}}$	0.2760	$C_{l_{\alpha_e}}$	0.0019 rad ⁻¹
$C_{l_{\alpha_e} \text{ diff}}$	0.1875	AR _a	4.32	$\Delta C_{l_{\alpha_e}}$	7.8049 rad ⁻¹	($\partial C_{l_{\alpha_e}} / \partial \alpha$)	0.1264	$C_{l_{\alpha_e}}$	-0.3659 rad ⁻¹
$X_{C_{l_{\alpha_e}}}$	62.73 %	$C_{l_{\alpha_e}}$	7.8049 rad ⁻¹	$C_{l_{\alpha_e}}$	-4.5029 rad ⁻¹	$C_{l_{\alpha_e}}$	0.8302 rad ⁻¹	$C_{l_{\alpha_e}}$	-0.3678 rad ⁻¹

Fig. 71 Yaw rate related derivatives

Airplane Lift Coefficient and Downwash at Alpha = 0: Flight Condition 1							
Input Parameters							
S_a	837.00 ft ²	$C_{l_{\alpha_{\text{ref}}}}$	0.1875	S_a	190.00 ft ²	η_{lift}	1.000
$C_{l_{\alpha_{\text{ref}}}}$	0.1875	$\Delta C_{l_{\alpha_{\text{ref}}}}$	0.0000	$C_{l_{\alpha_{\text{ref}}}}$	5.7070 rad ⁻¹	$\alpha_{l_{\alpha_{\text{ref}}}}$	0.0 deg
Output Parameters							
α_{clean}	-1.6 deg	$\Delta C_{l_{\alpha_{\text{ref}}}}$	0.0000	$C_{l_{\alpha_{\text{ref}}}}$	-0.0178	$C_{l_{\alpha_{\text{ref}} \text{ clean}}}$	0.1875
α_a	-1.6 deg	$\Delta C_{l_{\alpha_{\text{ref}}}}$	0.0000	$C_{l_{\alpha_{\text{ref}} \text{ emp clean}}}$	0.1875	$C_{l_{\alpha_{\text{ref}} \text{ diff}}}$	0.1698

Fig. 72 Angle of attack related derivatives

Elevator Related Derivatives: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	$C_{l_{\alpha_e}}$	0.1698	$\dot{\alpha}_e$	0.60	S_a	190.00 ft ²	$\Delta C_{l_{\alpha_e}}$	0.0 deg
ΔT	0.0 deg F	S_a	837.00 ft ²	$C_{l_{\alpha_e}(\bar{M}=0)}$	6.2504 rad ⁻¹	AR _a	7.00	η_{lift}	1.000
U_1	350.00 kts	AR _a	8.00	$\tilde{C}_{l_{\alpha_e}}$	6.2504 rad ⁻¹	$\dot{\alpha}_e$	1.00	$(\partial C_{l_{\alpha_e}} / \partial \alpha)$	12.0 %
M_1	0.594	$C_{l_{\alpha_e}}$	7.7681 rad ⁻¹	$C_{l_{\alpha_e}}$	7.7681 rad ⁻¹	$C_{l_{\alpha_e}}$	1.2955 rad ⁻¹	$\alpha_{l_{\alpha_e}}$	0.4231
Output Parameters									
$C_{l_{\alpha_e}}$	0.594	$C_{l_{\alpha_e}}$	7.7681 rad ⁻¹	$C_{l_{\alpha_e}}$	7.7681 rad ⁻¹	$C_{l_{\alpha_e}}$	1.2955 rad ⁻¹	$C_{l_{\alpha_e}}$	0.0204 rad ⁻¹
$C_{l_{\alpha_e}}$	0.594	$C_{l_{\alpha_e}}$	7.7681 rad ⁻¹	$C_{l_{\alpha_e}}$	7.7681 rad ⁻¹	$C_{l_{\alpha_e}}$	1.2955 rad ⁻¹	$C_{l_{\alpha_e}}$	0.0087 rad ⁻¹

Fig. 73 Elevator related derivatives

Elevator Related Derivatives: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	$C_{l_{\alpha_e}}$	6.2504 rad ⁻¹	$\dot{\alpha}_e$	1.00	$(\partial C_{l_{\alpha_e}} / \partial \alpha)$	12.0 %	η_{lift}	95.0 %
ΔT	0.0 deg F	$C_{l_{\alpha_e}(\bar{M}=0)}$	6.2504 rad ⁻¹	$\Delta C_{l_{\alpha_e}}$	0.0 deg	$C_{l_{\alpha_e}}$	5.7070 rad ⁻¹	$\dot{\alpha}_e$	-0.04 deg
U_1	350.00 kts	S_a	190.00 ft ²	η_{lift}	1.000	$C_{l_{\alpha_e}}$	28.5 %	$(\partial C_{l_{\alpha_e}} / \partial \alpha)$	0.00 %
S_a	837.00 ft ²	AR _a	7.00	$(\partial C_{l_{\alpha_e}} / \partial \alpha)$	12.0 %	η_{lift}	0.05	$(C_l / C_{l_{\alpha_e}})_{\text{max}}$	
Output Parameters									
M_1	0.594	$C_{l_{\alpha_e}}$	7.7681 rad ⁻¹	V_a	1.0000	$\dot{\alpha}_e$	0.4231	$C_{l_{\alpha_e}}$	0.5482 rad ⁻¹
$C_{l_{\alpha_e}}$	7.7681 rad ⁻¹	$C_{l_{\alpha_e}}$	1.2955 rad ⁻¹	$\dot{\alpha}_e$	1.00	$C_{l_{\alpha_e}}$	2.4149 rad ⁻¹	$\alpha_{l_{\alpha_e}}$	0.4231
$C_{l_{\alpha_e}}$	7.7681 rad ⁻¹	$C_{l_{\alpha_e}}$	1.2955 rad ⁻¹	$C_{l_{\alpha_e}}$	1.2955 rad ⁻¹	$C_{l_{\alpha_e}}$	2.4149 rad ⁻¹	$C_{l_{\alpha_e}}$	-0.0003

Fig. 74 Elevator related derivatives

Elevator Related Derivatives: Flight Condition 1										
Input Parameters										
Altitude	30000	ft	$\dot{\alpha}_e$	0.60	$C_{\delta_e} @ M=0$	6.2504 rad ⁻¹	$(\delta C)_e$	12.0 %	δ_e	5.0 %
ΔT	0.0	deg F	$\Delta \alpha_{L_d}$	0.0 deg	S_a	190.00 rad ⁻¹	$(\delta C)_e$	12.0 %	δ_e	95.0 %
U_1	350.00	kts	$X_{gap}_{L_d}$	23.00 ft	ΔR_e	7.00	C_{δ_e}	5.7070 rad ⁻¹	δ_e	0.04 deg
S_w	837.00	rad ⁻¹	X_{gap}	24.32 ft	$\dot{\alpha}_e$	1.00	X_{gap}	61.30 ft	$(gapC)_e$	0.00 %
AR_w	9.00		$C_{\delta_e} @ M=0$	6.2504 rad ⁻¹	θ_{ref}	1.000	S_w / δ_e	28.5 %	Balance _e	0.05
									$(C_e / C_w)_{min}$	
									$(C_e / C_w)_{max}$	

Output Parameters										
M_1	0.594		C_{δ_e}	7.7681 rad ⁻¹	\dot{V}_1	0.8040	V_e	1.0000	$\dot{\alpha}_e$	0.4231
$C_{\delta_e} @ M=0$	7.7681 rad ⁻¹		C_{δ_e}	0.0702	C_{δ_e}	-4.5884 rad ⁻¹	$\dot{\alpha}_e$	1.00	C_{δ_e}	-1.9416 rad ⁻¹
									C_{δ_e}	-1.9416 rad ⁻¹

Fig. 75 Elevator related derivatives

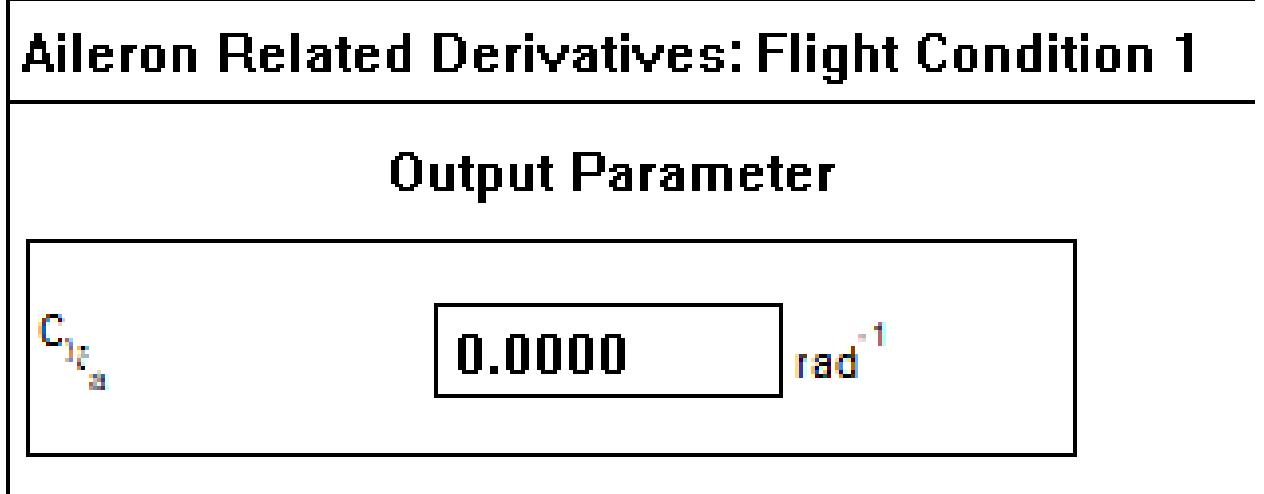


Fig. 76 Aileron related derivatives

Aileron Related Derivatives: Flight Condition 1										
Input Parameters										
Altitude	30000	ft	$\dot{\alpha}_a$	0.60	$C_{\delta_a} @ M=0$	6.3598 rad ⁻¹	$(\delta C)_a$	98.0 %	δ_a	0.0 deg
ΔT	0.0	deg F	$\Delta \alpha_{L_d}$	0.0 deg	$C_{\delta_a} @ M=0$	6.3598 rad ⁻¹	$(gapC)_a$	2.00 %	Number δ_a	3
U_1	350.00	kts	$(\delta C)_a$	12.00 %	C_w / δ_a	23.8 %	Balance _a	0.05	$\delta_{a,min}$	
AR_w	8.00		$(\delta C)_a$	12.00 %	$\dot{\alpha}_a$	60.0 %	$\delta_a / \dot{\alpha}_a$	1.0000	$\delta_{a,max}$	

Output Parameters										
M_1	0.594		C_{δ_a}	7.9041 rad ⁻¹	$t_{ref,a}$	0.85	C_a	0.0000	V_a	1.0000
\dot{q}_1	155.41	ft/s	$\dot{\alpha}_a$	0.0 deg	C_{δ_a}	0.0000	K_{δ_a}	1.0000	C_{δ_a}	0.0814 rad ⁻¹
$C_{\delta_a} @ M=0$	7.9041 rad ⁻¹		$\dot{\alpha}_a$	0.00 deg	C_{δ_a}	0.0000	C_{δ_a}	0.0814 rad ⁻¹	C_{δ_a}	0.1629 rad ⁻¹

Fig. 77 Aileron related derivatives

Aileron Related Derivatives: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	α_{ref}	-3.0 deg	AR_w	8.00	$(\partial C)_{\alpha}$	12.00 %	η_z	60.0 %
ΔT	0.0 deg F	ω	-1.0 deg	λ_{wz}	0.60	$C_{\alpha_{\text{ref}} \text{DM-0}}$	6.3598 rad ⁻¹	η_{α_z}	98.0 %
U_1	350.00 kts	$C_{\alpha_{\text{ref}} \text{chem}}$	5.3706 rad ⁻¹	λ_{wz}	0.0 deg	$C_{\alpha_{\text{ref}} \text{DM-0}}$	6.3598 rad ⁻¹	$(\text{gap}C)_z$	2.00 %
α	0.00 deg	S_w	837.00 m ²	$(\partial C)_{\alpha}$	12.00 %	$C_{\alpha/\alpha}$	23.8 %	Balance _z	0.05
								Number $\tilde{\alpha}_z$	3
Output Parameters									
M_1	0.594	$C_{\alpha_{\text{ref}}}$	7.9041 rad ⁻¹	η_z	0.00 deg	$C_{\alpha_{\beta}}$	0.0000	C_{α_z}	0.0000
\tilde{q}_1	155.41 lbf/in ²	$C_{\alpha_{\text{ref}} \text{DM-0}}$	0.1875	λ_{wz}	0.85	$C_{\alpha_{\beta}}$	0.0000	C_{α_z}	0.0000
$C_{\alpha_{\text{ref}}}$	7.9041 rad ⁻¹	λ_z	0.0 deg	$C_{\alpha_{\beta}}$	0.0000	C_{α_z}	0.0000	$C_{\alpha_{\text{ref}}}$	0.0044 rad ⁻¹

Fig. 78 Aileron related derivatives

Rudder Related Derivative: Flight Condition 1									
Input Parameters									
Altitude	30000 ft	S_w	190.00 m ²	AR_w	3.00	$(\partial C)_{\alpha}$	1.00	η_z	2.00 %
ΔT	0.0 deg F	$X_{\alpha_{\text{ref}}}$	61.30 ft	λ_{wz}	0.80	$(\partial C)_{\alpha}$	12.0 %	η_{α_z}	1.000 %
U_1	350.00 kts	$Z_{\alpha_{\text{ref}}}$	6.00 ft	λ_{wz}	5.0 deg	$(\partial C)_{\alpha}$	12.0 %	$(\text{gap}C)_z$	28.5 %
S_w	837.00 m ²	$Z_{\alpha_{\text{ref}}}$	5.00 ft	$C_{\alpha_{\text{ref}} \text{DM-0}}$	6.2800 rad ⁻¹	$X_{\alpha_{\text{ref}}}$	60.00 ft	η_z	5.0 %
AR_w	8.00	S_w	137.00 m ²	$C_{\alpha_{\text{ref}} \text{DM-0}}$	6.2800 rad ⁻¹	$Z_{\alpha_{\text{ref}}}$	15.00 ft	η_{α_z}	95.0 %
								Number $\tilde{\alpha}_z$	2
Output Parameters									
M_1	0.594	$C_{\alpha_{\text{ref}}}$	7.8049 rad ⁻¹	C_{α_z}	-4.5029 rad ⁻¹	η_z	0.85	B_0	0.4356
\tilde{q}_1	155.41 lbf/in ²	$C_{\alpha_{\text{ref}}}$	7.8049 rad ⁻¹	X_{α_z}	0.2760	B_{α_z}	0.4356	C_{α_z}	0.2717 rad ⁻¹
AR_w	4.32	$C_{\alpha_{\text{ref}}}$	7.8049 rad ⁻¹	η_z	1.0000	C_{α_z}	0.2717 rad ⁻¹	$C_{\alpha_{\text{ref}}}$	0.0000

Fig. 79 Rudder related derivatives

Rudder Related Derivatives: Flight Condition 1									
Input Parameters									
α	0.00 deg	$C_{\alpha_{\text{ref}}}$	0.2717 rad ⁻¹	AR_w	8.00	η_z	0.80	$Z_{\alpha_{\text{ref}}}$	15.00 ft
$X_{\alpha_{\text{ref}}}$	24.32 ft	$C_{\alpha_{\text{ref}}}$	0.2717 rad ⁻¹	S_w	137.00 m ²	λ_{wz}	5.0 deg	$(\text{gap}C)_z$	28.5 %
$Z_{\alpha_{\text{ref}}}$	2.95 ft	S_w	837.00 m ²	AR_w	3.00	$X_{\alpha_{\text{ref}}}$	60.00 ft	η_z	5.0 %
								Balance _z	0.05
Output Parameters									
$C_{\alpha_{\text{ref}}}$	0.0726 rad ⁻¹	C_{α_z}	0.0726 rad ⁻¹	$C_{\alpha_{\text{ref}}}$	0.0000				

Fig. 80 Rudder related derivatives

Rudder Related Derivatives: Flight Condition 1									
Input Parameters									
α	0.00 deg	$C_{\alpha_{\text{ref}}}$	0.2717 rad ⁻¹	AR_w	8.00	η_z	0.80	$Z_{\alpha_{\text{ref}}}$	15.00 ft
$X_{\alpha_{\text{ref}}}$	24.32 ft	$C_{\alpha_{\text{ref}}}$	0.2717 rad ⁻¹	S_w	137.00 m ²	λ_{wz}	5.0 deg	$(\text{gap}C)_z$	28.5 %
$Z_{\alpha_{\text{ref}}}$	2.95 ft	S_w	837.00 m ²	AR_w	3.00	$X_{\alpha_{\text{ref}}}$	60.00 ft	η_z	5.0 %
								Balance _z	0.05
Output Parameters									
$C_{\alpha_{\text{ref}}}$	-0.1380 rad ⁻¹	C_{α_z}	-0.1380 rad ⁻¹	$C_{\alpha_{\text{ref}}}$	0.0000				

Fig. 81 Rudder related derivatives

B. AAA: Static Stability and One Engine Inoperative Analyses

Angle of Attack Related Derivatives: Pitching Moment: Flight Condition 1														
Input Parameters														
Altitude	30000	ft	δ_{AOA}	0.93	X_{AOA}	23.00	ft	S_b	190.00	ft^2				
ΔT	0.0	deg F	S_h	837.00	π^2	V_{AOA}	0.00	ft	V_{AOA}	0.00	ft			
U_1	350.00	fts	AR_w	8.00	$(\text{IC})_w$	12.00	%	b_0	1.00	$(\text{IC})_b$	12.0	%		
$C_{L_{\text{AOA}} \text{ (M=0)}}$	6.3598	rad ⁻¹	λ_{AOA}	0.60	$(\text{IC})_b$	12.00	%	λ_{AOA}	0.0	deg	Z_{AOA}	6.00	ft	
$C_{L_{\text{AOA}} \text{ (M=0)}}$	6.3598	rad ⁻¹	λ_{AOA}	0.0	deg	Z_{AOA}	2.00	ft	X_{AOA}	60.00	ft			
Output Parameters														
M_1	0.594		$C_{L_{\text{AOA}}}$	7.9041	rad ⁻¹	$C_{L_{\text{AOA}}}$	5.3706	rad ⁻¹	Z_{AOA}	0.2049	Z_{AOA}	3.6121		
R_t	155.41	ft	$C_{L_{\text{AOA}}}$	7.9041	rad ⁻¹	$C_{L_{\text{AOA}}}$	5.3724	rad ⁻¹	δ_{AOA}	7.7681	rad ⁻¹	$C_{L_{\text{AOA}}}$	5.7070	rad ⁻¹
X_{AOA}	0.0702		$C_{L_{\text{AOA}}}$	7.9041	rad ⁻¹	X_{AOA}	26.20	ft	$C_{L_{\text{AOA}}}$	7.7681	rad ⁻¹	$C_{L_{\text{AOA}}}$	0.7062	rad ⁻¹
Z_w	10.44	ft	$C_{L_{\text{AOA}}}$	5.3706	rad ⁻¹	Z_{AOA}	0.2500	ft	$C_{L_{\text{AOA}}}$	7.7681	rad ⁻¹	Z_{AOA}	6.00	ft
X_{AOA}	0.59	ft	$C_{L_{\text{AOA}}}$	5.3724	rad ⁻¹	X_{AOA}	25.73	ft	X_{AOA}	61.30	ft	Z_{AOA}	0.3931	
High Lift Devices Table											\bar{Z}_w	0.6399		
#	High Lift Device	η_1 %	η_0 %	δ_{AOA} %	δ deg						C_v	3.5082	rad ⁻¹	
1	Single Slotted Flap	9.0	55.5	30.0	0.0									

Fig. 82 Angle of attack related derivatives

Sideslip Related Derivatives: Yawing Moment: Flight Condition 1															
Input Parameters															
Altitude	30000	ft	δ_{AOA}	0.60	Z_{AOA}	6.00	ft	X_{AOA}	60.00	ft					
ΔT	0.0	deg F	λ_{AOA}	0.0	deg	Z_{AOA}	5.00	ft	Z_{AOA}	15.00	ft				
U_1	350.00	fts	Z_{AOA}	2.00	ft	S_b	137.00	ft^2	δ_{AOA}	6.2800	rad ⁻¹				
α	0.00	deg	Z_{AOA}	2.50	ft	AR_w	3.00		$C_{L_{\text{AOA}} \text{ (M=0)}}$	6.2800	rad ⁻¹				
S_w	837.00	π^2	S_h	190.00	π^2	δ_w	0.80		δ_{AOA}	1.00					
AR_w	9.00		X_{AOA}	61.30	ft	λ_{AOA}	5.0	deg	$(\text{IC})_b$	12.0	%				
Output Parameters															
M_1	0.594		Z_{AOA}	24.76	ft	$C_{L_{\text{AOA}}}$	7.8049	rad ⁻¹	λ_{AOA}	0.2760	K_{AOA}	-0.00029	$C_{L_{\text{AOA}}}$	0.3897	rad ⁻¹
R_t	93.1248	$\times 10^3$	AR_{ref}	4.32		$C_{L_{\text{AOA}}}$	7.8049	rad ⁻¹	$(\text{IC})_b$	-0.1264	K_{AOA}	1.92878	C_v	0.3995	rad ⁻¹
X_{AOA}	62.73	ft	$C_{L_{\text{AOA}}}$	7.8049	rad ⁻¹	$C_{L_{\text{AOA}}}$	-4.5029	rad ⁻¹	$C_{L_{\text{AOA}}}$	0.8302	rad ⁻¹	$C_{L_{\text{AOA}}}$	0.0098	rad ⁻¹	

Fig. 83 Sideslip related derivatives

Rudder Related Derivatives: Flight Condition 1														
Input Parameters														
α	0.00	deg	$C_{L_{\text{AOA}}}$	0.2717	rad ⁻¹	AR_w	8.00		δ_w	0.80	Z_{AOA}	15.00	ft	
X_{AOA}	24.32	ft	$C_{L_{\text{AOA}}}$	0.2717	rad ⁻¹	S_b	137.00	ft^2	λ_{AOA}	5.0	deg	δ_w	28.5	%
Z_w	2.95	ft	S_h	837.00	π^2	AR_w	3.00		$(\text{IC})_b$	12.0	%	b_0	0.82	deg
Z_w	2.95	ft	X_{AOA}	61.30	ft	λ_{AOA}	5.0	deg	X_{AOA}	24.32	ft	w_{max}	6.78	ft
Output Parameters														
$C_{L_{\text{AOA}}}$	-0.1380	rad ⁻¹	$C_{L_{\text{AOA}}}$	-0.1380	rad ⁻¹	$C_{L_{\text{AOA}}}$	0.0000							

Fig. 84 Rudder related derivatives

Engine Out Control: Flight Condition 1													
Input Parameters													
Altitude	30000 ft	ΔT	0.0 deg F	S_w	837.00 ft ²	AR_w	8.00	V_S	350.00 kts				
Output Parameters													
V_{mc}	420.00 kts	δ_e	0.28 deg										
Propeller Table													
#	Type	SHP set hp	X _{prop} ft	Y _{prop} ft	Z _{prop} ft	i _{prop} deg	ψ prop deg	η _{prop}	K _{loss} %	C _D _{prop_wm}	C _D _{prop_stop}	P _{avail} hp	T _{avail} lb
1	Propeller: On	1555	22.00	9.01	4.00	7.0	0.0	0.850	5.7	0.0000	0.0000	1246	1160
2	Propeller: On	0	22.00	-9.01	4.00	7.0	0.0	0.850	5.7	0.0000	0.0000	0	0

Fig. 85 One engine out at cruise altitude and speed

Engine Out Control: Flight Condition 1													
Input Parameters													
Altitude	7000 ft	ΔT	0.0 deg F	S_w	837.00 ft ²	AR_w	8.00	V_S	140.00 kts				
Output Parameters													
V_{mc}	168.00 kts	δ_e	0.82 deg										
Propeller Table													
#	Type	SHP set hp	X _{prop} ft	Y _{prop} ft	Z _{prop} ft	i _{prop} deg	ψ prop deg	η _{prop}	K _{loss} %	C _D _{prop_wm}	C _D _{prop_stop}	P _{avail} hp	T _{avail} lb
1	Propeller: On	1555	22.00	9.01	4.00	7.0	0.0	0.850	5.7	0.0000	0.0000	1246	1160
2	Propeller: On	0	22.00	-9.01	4.00	7.0	0.0	0.850	5.7	0.0000	0.0000	0	0

Fig. 86 One engine out at takeoff altitude and speed

C. AAA: Transfer Function and Flying Quality Analyses

Computation of Longitudinal Transfer Functions: Flight Condition 1										
Input Parameters										
Altitude	30000 ft	α	0.00 deg	C_{l_u}	0.0106	$C_{l_{T_2}}$	0.0038	C_{l_b}	3.6077 rad ⁻¹	
ΔT	0.0 deg F	γ	0.0 deg	C_{n_u}	-3.5082 rad ⁻¹	$C_{n_{T_2}}$	-0.0251 rad ⁻¹	C_{n_b}	14.1354 rad ⁻¹	
\dot{U}_1	350.00 kts	$\dot{\theta}_{\omega}$	10.44 ft	C_{r_u}	-12.7779 rad ⁻¹	$C_{r_{T_2}}$	0.1076	C_{r_b}	0.0177	
$W_{current}$	37689.0 lb	\dot{V}_D	51880.2 slug ft ²	$C_{C_{D_w}}$	-32.5032 rad ⁻¹	$C_{C_{D_{T_2}}}$	0.0586	$C_{C_{D_b}}$	0.0972 rad ⁻¹	
S_w	837.00 ft ²	C_{l_1}	0.0013	$C_{l_{T_1}}$	-0.0013	C_{l_b}	6.1586 rad ⁻¹	$C_{l_{D_b}}$	0.0000	
Output Parameters										
M_1	0.594	X_u	1.1436 $\frac{ft}{s}$	M_{T_u}	0.0001 $\frac{1}{ft}$	$B_{u_{D}}$	8860.1	C_{B_D}	0.581	
G_1	155.41	Z_u	-0.0510 $\frac{ft}{s}$	M_b	-91.8437 $\frac{1}{ft}$	$C_{u_{D}}$	58549.8	$B_{u_{D}}$	0.0530 $\frac{1}{ft}$	
W/S	45.03	Z_u	679.4278 $\frac{1}{ft}$	M_{T_b}	0.6576 $\frac{1}{ft}$	$B_{u_{D}}$	595.4	C_{B_D}	0.093	
θ	0.0 deg	Z_b	-3.5074 $\frac{1}{ft}$	M_b	-2.9565 $\frac{1}{ft}$	$E_{u_{D}}$	164.2	$B_{u_{D}}$	0.0000 $\frac{1}{ft}$	
X_u	-0.0066 s ⁻¹	Z_b	-13.7427 $\frac{1}{ft}$	M_z	-7.5205 s ⁻¹	$RH_{u_{D}}$	23122811400.2	$C_{u_{D}}$	Z_u	-60.3020 $\frac{1}{ft}$
X_T	-0.0033 s ⁻¹	M_u	0.0006 $\frac{1}{ft}$	$A_{u_{D}}$	594.2	$B_{u_{D}}$	9.9203 $\frac{1}{ft}$	$T_{C_{u_{D}}}$	M_u	-50.8298 $\frac{1}{ft^2}$

Fig. 87 Longitudinal transfer functions, frequencies, and damping

Lateral-Directional Transfer Functions: Flight Condition 1									
Input Parameters									
W_{gross}	37689.0	b	S_a	837.00	rad^2	I_{z_0}	200121.1	$\text{slug}\cdot\text{ft}^2$	C_{y_0}
Altitude	30000	ft	θ	0.0	deg	I_{z_0}	245693.0	$\text{slug}\cdot\text{ft}^2$	C_{z_0}
ΔT	0.0	deg F	α	0.00	deg	I_{z_0}	4375.6	$\text{slug}\cdot\text{ft}^2$	C_{β_0}
U_1	350.00	kts	R_a	81.83	ft	C_{y_0}	-0.3025	rad^{-1}	$C_{y_{10}}$
Output Parameters									
M_1	0.594		Y_{T_0}	-100.9659	$\frac{1}{s}$	L	0.9809	s^{-1}	$B_{\text{ail-dr}}$
q_1	155.41	$\frac{\text{ft}}{\text{s}^2}$	Y_{T_0}	0.0000	$\frac{1}{s}$	N_b	17.3067	s^{-2}	$C_{\text{ail-dr}}$
WS	45.03	$\frac{\text{ft}}{\text{s}}$	Y_c	-1.0227	$\frac{1}{s}$	N_{T_0}	0.0000	s^{-2}	$D_{\text{ail-dr}}$
I_{y_0}	200121.1	$\text{slug}\cdot\text{ft}^2$	Y_c	5.9385	$\frac{1}{s}$	$E_{\text{ail-dr}}$	24.8		T_b
I_{z_0}	245693.0	$\text{slug}\cdot\text{ft}^2$	I_{z_0}	-16.0899	s^{-2}	$R_{\text{ail-dr}}$	197293681276.6		T_R
I_{z_0}	4375.6	$\text{slug}\cdot\text{ft}^2$	I_y	-1.9372	s^{-1}	$A_{\text{ail-dr}}$	590.5		V_{T_0}
CU Boulder Advanced Aircraft Analysis 4.0 Project 12/12/18 10:34 am									

Fig. 88 Lateral-directional transfer functions, frequencies, and damping response to ailerons

Lateral-Directional Transfer Functions: Flight Condition 1									
Input Parameters									
W_{gross}	37689.0	b	S_a	837.00	rad^2	I_{z_0}	200121.1	$\text{slug}\cdot\text{ft}^2$	C_{y_0}
Altitude	30000	ft	θ	0.0	deg	I_{z_0}	245693.0	$\text{slug}\cdot\text{ft}^2$	C_{z_0}
ΔT	0.0	deg F	α	0.00	deg	I_{z_0}	4375.6	$\text{slug}\cdot\text{ft}^2$	C_{β_0}
U_1	350.00	kts	R_a	81.83	ft	C_{y_0}	-0.3025	rad^{-1}	$C_{y_{10}}$
Output Parameters									
M_1	0.594		Y_{T_0}	-100.9659	$\frac{1}{s}$	L	0.9809	s^{-1}	$B_{\text{ail-dr}}$
q_1	155.41	$\frac{\text{ft}}{\text{s}^2}$	Y_{T_0}	0.0000	$\frac{1}{s}$	N_b	17.3067	s^{-2}	$C_{\text{ail-dr}}$
WS	45.03	$\frac{\text{ft}}{\text{s}}$	Y_c	-1.0227	$\frac{1}{s}$	N_{T_0}	0.0000	s^{-2}	$D_{\text{ail-dr}}$
I_{y_0}	200121.1	$\text{slug}\cdot\text{ft}^2$	Y_c	5.9385	$\frac{1}{s}$	$E_{\text{ail-dr}}$	24.8		T_b
I_{z_0}	245693.0	$\text{slug}\cdot\text{ft}^2$	I_{z_0}	-16.0899	s^{-2}	$R_{\text{ail-dr}}$	197293681276.6		T_R
I_{z_0}	4375.6	$\text{slug}\cdot\text{ft}^2$	I_y	-1.9372	s^{-1}	$A_{\text{ail-dr}}$	590.5		V_{T_0}
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Fig. 89 Lateral-directional transfer functions, frequencies, and damping response to rudder

Longitudinal Mode Checking Flight Phase Category B: Flight Condition 1							
Input Parameters							
ω_{fp}	9.9203	$\frac{1}{\text{rad}}$	ζ_{fp}	0.581		$\omega_{\text{fp, long}}$	0.0530 $\frac{1}{\text{rad}}$
Output Parameters							
n/α	21.316	$\frac{1}{\text{rad}}$	T_{fp}		s	T_{Vfp}	140.700 s
						Level $\zeta_{fp} = 1$	Level $\zeta_{fp} = 2$

Fig. 90 Longitudinal mode frequencies, phugoid and short period flying quality levels

Roll Mode Performance Checking Flight Phase Category B, Cruise: Flight Condition 1									
Input Parameters									
Altitude	30000	ft	U_1	350.00	kts	ω_s	81.83	rad	C_{y_0}
									-0.5259 rad ⁻¹
ΔT	0.0	deg F	S_a	837.00	in ²	ω_{z_0}	200121.1	slug·ft ²	C_{z_0}/C_{x_0}
									23.8 %
									$\omega_{z_{max}}$
									25.0 deg
									t_{roll}
									1.9 s
Output Parameters									
Level $T_{z_0} = 1$			Level $\dot{\phi}_0 = 1$			θ_{roll}	115.3	deg	

Fig. 91 Roll mode performance and flying quality level

Spiral and Dutch Roll Mode Checking Flight Phase Category B,Cruise: Flight Condition 1									
Input Parameters									
Altitude	30000	ft	S_a	837.00	in ²	ω_s	245693.0	slug·ft ²	C_{y_0}
									-0.0193 rad ⁻¹
ΔT	0.0	deg F	ω_s	81.83	rad	ω_{z_0}	4375.6	slug·ft ²	C_{z_0}
									-0.3678 rad ⁻¹
U_1	350.00	kts	ω_s	200121.1	slug·ft ²	C_{y_0}	0.3995	rad ⁻¹	C_{z_0}
									-0.3025 rad ⁻¹
									$\omega_{z_{max}}$
									4.1464 rad
Output Parameters									
σR_0	0.8797		T_{z_0}		s	$T_{\dot{\phi}_0}$	581.996	s	Level $\dot{\phi}_0 = \text{Stable}$
									Level $\dot{\phi}_0 = 1$
									Level $\omega_{z_0} = 1$
									Level $\omega_{z_0}/\dot{\phi}_0 = 1$

Fig. 92 Spiral and dutch roll fling quality levels

Spiral and Dutch Roll Mode Checking Flight Phase Category B,Cruise: Flight Condition 1									
Input Parameters									
Altitude	30000	ft	S_a	837.00	in ²	ω_s	245693.0	slug·ft ²	C_{y_0}
									-0.0193 rad ⁻¹
ΔT	0.0	deg F	ω_s	81.83	rad	ω_{z_0}	4375.6	slug·ft ²	C_{z_0}
									-0.3678 rad ⁻¹
U_1	350.00	kts	ω_s	200121.1	slug·ft ²	C_{y_0}	0.3995	rad ⁻¹	C_{z_0}
									-0.3025 rad ⁻¹
									$\omega_{z_{max}}$
									4.1464 rad
Output Parameters									
σR_0	0.8797		T_{z_0}		s	$T_{\dot{\phi}_0}$	581.996	s	Level $\dot{\phi}_0 = \text{Stable}$
									Level $\dot{\phi}_0 = 1$
									Level $\omega_{z_0} = 1$
									Level $\omega_{z_0}/\dot{\phi}_0 = 1$

Fig. 93 Spiral and dutch roll fling quality levels